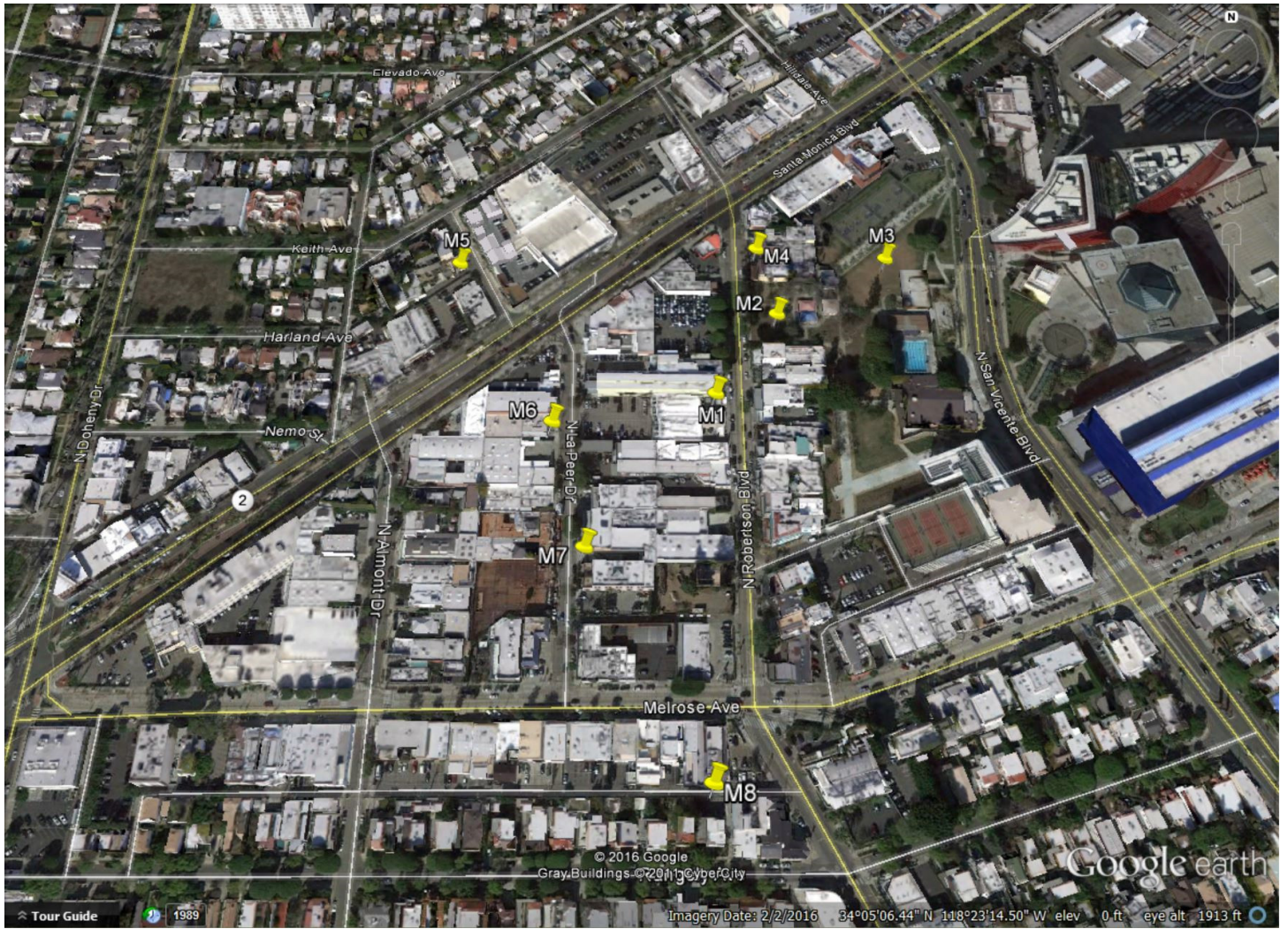


# **APPENDIX H**

## *Noise Impact Modeling Data*







**M1 – Project Site**

**655 North Robertson Blvd West Hollywood, California 90069**

# FIELD NOISE MEASUREMENT DATA

DUDEK

PROJECT	Robertson Lane		PROJECT #	8595
SITE ID	M11			
SITE ADDRESS	655 N. Robertson Blvd West Hollywood, CA 90069			
START DATE	2/25/15	END DATE	2/25/15	
START TIME	2:29pm	END TIME	2:44pm	
OBSERVER(S)	Stephanie Tang			

<b>METEOROLOGICAL CONDITIONS</b>									
TEMP	74.0	F	HUMIDITY	45.1	% R.H.	WIND	CALM	<u>LIGHT</u>	MODERATE
WINDSPD	1.0	MPH	DIR.	N	NE	S	SE	S	SW
SKY	<u>SUNNY</u>	CLEAR	OVRCAST	<u>PRTLY CLDY</u>	FOG	RAIN	VARIABLE	STEADY	GUSTY
<b>ACOUSTIC MEASUREMENTS</b>									
MEAS. INSTRUMENT	Piccolo SLM				TYPE	1	<u>2</u>	SERIAL #	120625008
CALIBRATOR	BSWA CA114				SERIAL #	490151			
CALIBRATION CHECK	PRE TEST	94.0	dBa SPL	POST-TEST	94.0	dBa SPL	WINDSCRN	<input checked="" type="checkbox"/>	
SETTINGS	<u>A-WTD</u>	<u>SLOW</u>	FAST	FRONTAL	RANDOM	ANSI	OTHER:		
REC. #	BEGIN	END	Leq	Lmax	Lmin	L90	L50	L10	OTHER (SPECIFY METRIC)
M1	2:29am	2:44pm	65.5	78.6	52.8				
<b>COMMENTS</b>									

<b>SOURCE INFO AND TRAFFIC COUNTS</b>										
PRIMARY NOISE SOURCE					<u>TRAFFIC</u>	AIRCRAFT	RAIL	INDUSTRIAL	OTHER:	
ROADWAY TYPE:					Robertson Blvd	DIST. TO RDWY C/L OR EOP: <u>~60'</u>				
TRAFFIC COUNT DURATION:					15	MIN	SPEED		MIN	
									SPEED	
COUNT 1 (OR RDWY 1)	DIRECTION	NB/EB	SB/WB	NB/EB	SB/WB	COUNT 2 (OR RDWY 2)	NB/EB	SB/WB	NB/EB	SB/WB
	AUTOS	85	73							
	MED TRKS	2	0							
	HVY TRKS	1	0							
	BUSES	0	0							
MOTRCLS	0	1								
SPEEDS ESTIMATED BY: RADAR / DRIVING THE PACE										
POSTED SPEED LIMIT SIGNS SAY: 30mph										
OTHER NOISE SOURCES (BACKGROUND): <u>DIST. AIRCRAFT</u> RUSTLING LEAVES <u>DIST. BARKING DOGS</u> <u>BIRDS</u> <u>DIST. INDUSTRIAL</u>										
DIST. KIDS PLAYING <u>DIST. CONVRSTNS</u> YELLING <u>DIST. TRAFFIC (LIST RDWYS BELOW)</u> DISTD GARDENERS/LANDSCAPING NOISE										
OTHER: <u>Vehicle Approaching noise Meter Measurement location; Dist. traffic off Santa Monica Blvd</u>										

<b>DESCRIPTION / SKETCH</b>									
TERRAIN	<u>HARD</u>	SOFT	MIXED	<u>FLAT</u>	OTHER:				
PHOTOS	<u>See Attached</u>								
<b>OTHER COMMENTS / SKETCH</b>									



**M2 – West Hollywood Park (Facing Robertson Blvd)  
647 N. San Vicente Blvd West Hollywood, California 90048**

# FIELD NOISE MEASUREMENT DATA

PROJECT Robertson Lane PROJECT # 8595  
 SITE ID M2 - West Hollywood Park (off Robertson Blvd)  
 SITE ADDRESS 6474 San Vicente Blvd West Hollywood, CA OBSERVER(S) Stephanie Tang  
 START DATE 2/25/15 END DATE 2/25/15  
 START TIME 3:32 pm END TIME 3:47 am 9:00 AM

METEOROLOGICAL CONDITIONS  
 TEMP 73.7 F HUMIDITY 50.7 % R.H. WIND CALM LIGHT MODERATE  
 WINDSPD 0.8 MPH DIR. N NE S SE S SW W NW VARIABLE STEADY GUSTY  
 SKY SUNNY CLEAR OVRCAST PRTLY CLDY FOG RAIN

ACOUSTIC MEASUREMENTS  
 MEAS. INSTRUMENT Piccolo SLM TYPE 1 (2) SERIAL # 130625008  
 CALIBRATOR BSWA CALL4 SERIAL # 490151  
 CALIBRATION CHECK PRE-TEST 94.0 dBA SPL POST-TEST 94.0 dBA SPL WINDSCRN ✓

SETTINGS A-WTD SLOW FAST FRONTAL RANDOM ANSI OTHER: \_\_\_\_\_

REC. #	BEGIN	END	Leq	Lmax	Lmin	L90	L50	L10	OTHER (SPECIFY METRIC)
<u>M2</u>	<u>3:32am</u>	<u>3:47am</u>	<u>66.0</u>	<u>82.9</u>	<u>56.2</u>				

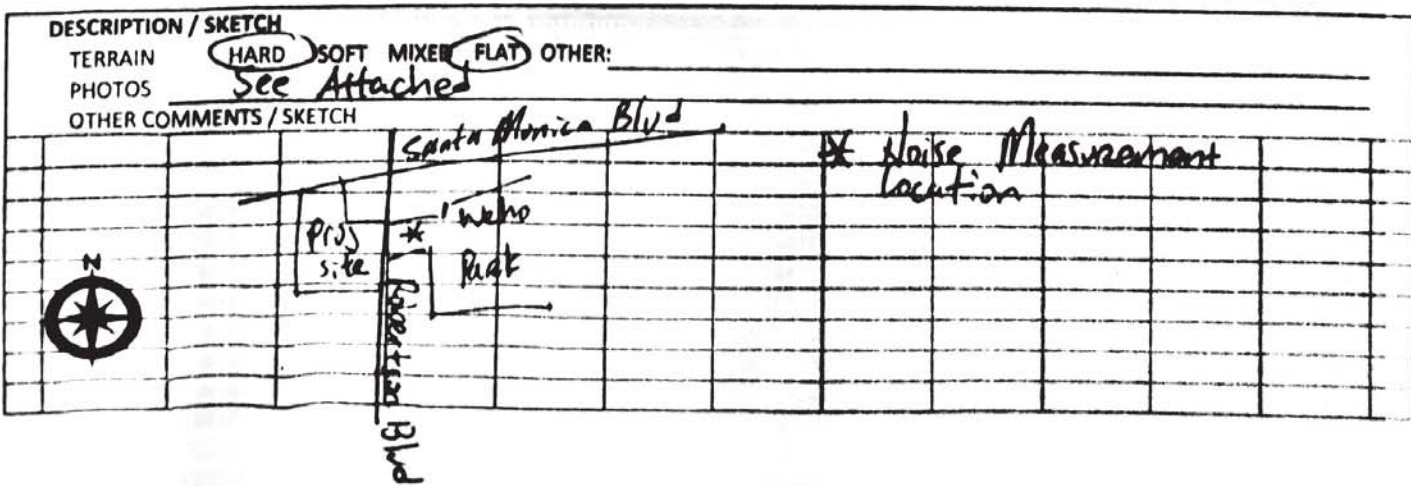
COMMENTS \_\_\_\_\_

SOURCE INFO AND TRAFFIC COUNTS  
 PRIMARY NOISE SOURCE TRAFFIC AIRCRAFT RAIL INDUSTRIAL OTHER: \_\_\_\_\_  
 ROADWAY TYPE: Robertson Blvd DIST. TO RDWY C/L OR EOP: ~80'  
 TRAFFIC COUNT DURATION: 15 MIN SPEED \_\_\_\_\_ MIN SPEED \_\_\_\_\_  

COUNT 1 (OR RDWY 1)	DIRECTION	NB/EB		SB/WB		IF COUNTING BOTH DIRECTIONS AS ONE, CHECK HERE	COUNT 2 (OR RDWY 2)	MIN		SPEED	
		NB/EB	SB/WB	NB/EB	SB/WB			NB/EB	SB/WB		
	AUTOS	<u>103</u>	<u>71</u>								
	MED TRKS	<u>1</u>	<u>0</u>								
	HVY TRKS	<u>1</u>	<u>0</u>								
	BUSES	<u>0</u>	<u>0</u>								
	MOTRCLS	<u>0</u>	<u>2</u>								

SPEEDS ESTIMATED BY: RADAR / DRIVING THE PACE  
 POSTED SPEED LIMIT SIGNS SAY: 30mph

OTHER NOISE SOURCES (BACKGROUND): DIST. AIRCRAFT RUSTLING LEAVES DIST. BARKING DOGS BIRDS DIST. INDUSTRIAL  
DIST. KIDS PLAYING DIST. CONVRTNS YELLING DIST. TRAFFIC (LIST RDWYS BELOW) DISTO GARDENERS/LANDSCAPING NOISE  
 OTHER: Dist traffic off Santa Monica Blvd





**M3 – West Hollywood Park (Facing San Vicente Blvd)  
647 N. San Vicente Blvd West Hollywood, California 90048**



# FIELD NOISE MEASUREMENT DATA

DUDEK

PROJECT Robertson Lane PROJECT # 8595  
 SITE ID M3 - West Hollywood Park (facing San Vicente)  
 SITE ADDRESS 477 N. San Vicente Blvd West Hollywood, CA OBSERVER(S) Stephanie Tang  
 START DATE 2/25/15 END DATE 2/25/15 ID # 90048  
 START TIME 13:59 AM END TIME 4:14

**METEOROLOGICAL CONDITIONS**

TEMP 70.9 F HUMIDITY 49.2 % R.H. WIND CALM LIGHT MODERATE  
 WINDSPD 10 MPH DIR. N NE S SE S SW W NW VARIABLE STEADY GUSTY  
 SKY SUNNY CLEAR OVRCAST PRTLY CLDY FOG RAIN

**ACOUSTIC MEASUREMENTS**

MEAS. INSTRUMENT Piccolo SLM TYPE 1 2 SERIAL # 130625008  
 CALIBRATOR BSWA CA114 SERIAL # 49015  
 CALIBRATION CHECK PRE-TEST 94.0 dBA SPL POST-TEST 94.0 dBA SPL WINDSCRN

**SETTINGS**

A-WTD  SLOW FAST FRONTAL RANDOM ANSI OTHER: \_\_\_\_\_

REC. #	BEGIN	END	Leq	Lmax	Lmin	L90	L50	L10	OTHER (SPECIFY METRIC)
<u>M3</u>	<u>3:59</u>	<u>4:14</u>	<u>62.6</u>	<u>78.7</u>	<u>56.6</u>				

**COMMENTS**

**SOURCE INFO AND TRAFFIC COUNTS**

PRIMARY NOISE SOURCE		TRAFFIC		AIRCRAFT	RAIL	INDUSTRIAL	OTHER:				
ROADWAY TYPE: <u>San Vicente Blvd</u>		SPEED					<u>~ 220'</u>				
TRAFFIC COUNT DURATION: <u>15</u> MIN		SPEED					MIN	SPEED			
COUNT 1 (OR RDWY 1)	DIRECTION	NB/EB	SB/WB	NB/EB	SB/WB	IF COUNTING BOTH DIRECTIONS AS ONE, CHECK HERE	COUNT 2 (OR RDWY 2)	NB/EB	SB/WB	NB/EB	SB/WB
	AUTOS	<u>209</u>	<u>191</u>								
MED TRKS	<u>3</u>	<u>8</u>									
HVY TRKS	<u>2</u>	<u>1</u>									
BUSES	<u>9</u>	<u>2</u>									
MOTRCLS	<u>1</u>	<u>1</u>									

SPEEDS ESTIMATED BY: RADAR / DRIVING THE PACE

POSTED SPEED LIMIT SIGNS SAY: 35 mph

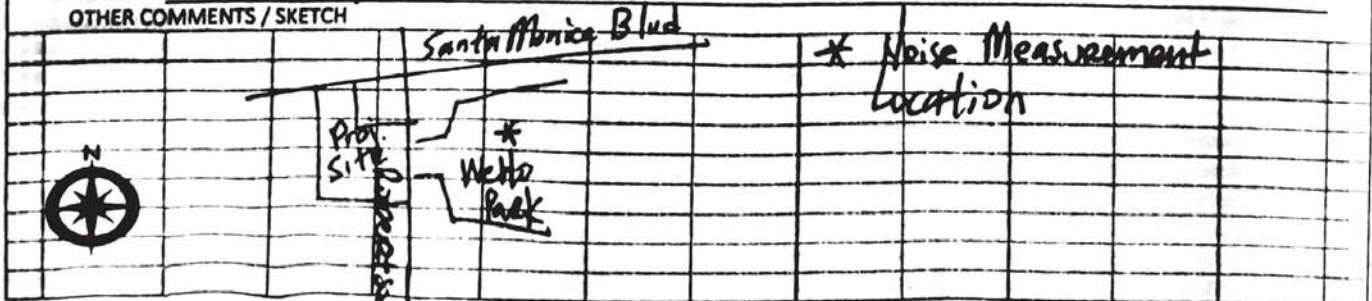
OTHER NOISE SOURCES (BACKGROUND): DIST. AIRCRAFT RUSTLING LEAVES DIST. BARKING DOGS BIRDS DIST. INDUSTRIAL  
DIST. KIDS PLAYING DIST. CONVRTNS / YELLING DIST. TRAFFIC (LIST RDWYS BELOW) DISTO GARDENERS/LANDSCAPING NOISE  
 OTHER: Dist traffic along Santa Monica Blvd

**DESCRIPTION / SKETCH**

TERRAIN  HARD  SOFT  MIXED  FLAT OTHER: \_\_\_\_\_

PHOTOS See Attached

OTHER COMMENTS / SKETCH





**M4 – The Abbey (Bar)**

**692 N. Robertson Blvd West Hollywood, California 90069**

# FIELD NOISE MEASUREMENT DATA

DUDEK

**PROJECT** Robertson Lane **PROJECT #** 8595  
**SITE ID** M4 - Abbey (Bar)  
**SITE ADDRESS** 692 N. Robertson Blvd West Hollywood **OBSERVER(S)** Stephanie Tang  
**START DATE** 2/25/15 **END DATE** 2/25/15 **9:00 AM**  
**START TIME** 4:41 AM **END TIME** 4:56 AM

**METEOROLOGICAL CONDITIONS**  
**TEMP** 70.9 F **HUMIDITY** 47.6 % R.H. **WIND** CALM LIGHT MODERATE  
**WINDSPD** 0.9 MPH **DIR.** N NE S SE S SW W NW **VARIABLE** STEADY GUSTY  
**SKY** STINNY CLEAR **OVRCAST** PRTLY CLDY FOG RAIN

**ACOUSTIC MEASUREMENTS**  
**MEAS. INSTRUMENT** Piccolo SLM **TYPE** 1 2 **SERIAL #** 130625008  
**CALIBRATOR** BSWA CALL4 **SERIAL #** 490157  
**CALIBRATION CHECK** **PRE-TEST** 94.0 dBA SPL **POST-TEST** 94.0 dBA SPL **WINDSCRN** ✓

**SETTINGS** A-WTD SLOW FAST FRONTAL RANDOM ANSI OTHER: \_\_\_\_\_

REC. #	BEGIN	END	Leq	Lmax	Lmin	L90	L50	L10	OTHER (SPECIFY METRIC)
<u>M4</u>	<u>4:41 AM</u>	<u>4:56 AM</u>	<u>73.0</u>	<u>80.9</u>	<u>66.6</u>				

**COMMENTS**  
 \_\_\_\_\_  
 \_\_\_\_\_

**SOURCE INFO AND TRAFFIC COUNTS**  
**PRIMARY NOISE SOURCE** TRAFFIC AIRCRAFT RAIL INDUSTRIAL OTHER: \_\_\_\_\_  
**ROADWAY TYPE:** Robertson Blvd **DIST. TO RDWY C/L OR EOP:** ~40'  
**TRAFFIC COUNT DURATION:** 15 MIN **SPEED** \_\_\_\_\_  
**MIN** \_\_\_\_\_ **SPEED** \_\_\_\_\_

COUNT 1 (OR RDWY 1)	DIRECTION	NB/EB		SB/WB		IF COUNTING BOTH DIRECTIONS AS ONE, CHECK HERE	COUNT 2 (OR RDWY 2)	NB/EB		SB/WB	
		NB/EB	SB/WB	NB/EB	SB/WB			NB/EB	SB/WB		
	AUTOS	<u>118</u>	<u>79</u>								
	MED TRKS	<u>0</u>	<u>0</u>								
	HVY TRKS	<u>0</u>	<u>0</u>								
	BUSES	<u>0</u>	<u>0</u>								
	MOTRCLS	<u>0</u>	<u>1</u>								

**SPEEDS ESTIMATED BY:** RADAR / DRIVING THE PACE  
**POSTED SPEED LIMIT SIGNS SAY:** 30 mph

**OTHER NOISE SOURCES (BACKGROUND):** DIST. AIRCRAFT RUSTLING LEAVES DIST. BARKING DOGS BIRDS DIST. INDUSTRIAL  
 DIST. KIDS PLAYING DIST. CONVRTNS / YELLING DIST. TRAFFIC (1ST RDWYS BELOW) DISTD GARDENERS/LANDSCAPING NOISE  
**OTHER:** Dist traffic off Santa Monica Blvd; Bar Music at Noise Measurement Location

**DESCRIPTION / SKETCH**  
**TERRAIN** HARD SOFT MIXED FLAT OTHER: \_\_\_\_\_  
**PHOTOS** See Attached  
**OTHER COMMENTS / SKETCH**



**M5 – Side of SFR Garage**

**715 Ramage Street West Hollywood, California 90069**

# FIELD NOISE MEASUREMENT DATA

DUDEK

PROJECT Robertson Lane PROJECT # 8595  
 SITE ID M5 - Side of SR Garage  
 SITE ADDRESS 715 Ramage St West Hollywood, CA 90069 OBSERVER(S) Stephanie Tang  
 START DATE 2/26/15 END DATE 2/26/15  
 START TIME 10:30AM END TIME 10:45AM

**METEOROLOGICAL CONDITIONS**

TEMP 67.6 F HUMIDITY 48.6 % R.H. WIND CALM LIGHT MODERATE  
 WINDSPD 0.9 MPH DIR. N NE S SE S SW W NW VARIABLE STEADY GUSTY  
 SKY SUNNY CLEAR OVRCAST PRTRY CLDY FOG RAIN

**ACOUSTIC MEASUREMENTS**

MEAS. INSTRUMENT Piccolo SLM TYPE 1 2 SERIAL # 130625008  
 CALIBRATOR BSWA CA 114 SERIAL # 490151  
 CALIBRATION CHECK PRE-TEST 94.0 dBA SPL POST-TEST 94.0 dBA SPL WINDSCRN ✓

SETTINGS A-WTD SLOW FAST FRONTAL RANDOM ANSI OTHER: \_\_\_\_\_

REC. #	BEGIN	END	Leq	Lmax	Lmin	L90	L50	L10	OTHER (SPECIFY METRIC)
<u>M5</u>	<u>10:30AM</u>	<u>10:45AM</u>	<u>62.0</u>	<u>69.4</u>	<u>53.1</u>				

COMMENTS \_\_\_\_\_

**SOURCE INFO AND TRAFFIC COUNTS**

PRIMARY NOISE SOURCE ROADWAY TYPE: Ramage St TRAFFIC AIRCRAFT RAIL INDUSTRIAL OTHER: \_\_\_\_\_  
 DIST. TO RDWY C/L OR EOP: ~55'

TRAFFIC COUNT DURATION: 15 MIN SPEED \_\_\_\_\_  
 MIN SPEED \_\_\_\_\_

COUNT 1 (OR RDWY 1)	DIRECTION	NB/EB		SB/WB		IF COUNTING BOTH DIRECTIONS AS ONE, CHECK HERE	COUNT 2 (OR RDWY 2)	NB/EB		SB/WB	
		NB/EB	SB/WB	NB/EB	SB/WB			NB/EB	SB/WB		
	AUTOS	<u>3</u>	<u>3</u>								
	MED TRKS	<u>1</u>	<u>1</u>								
	HVY TRKS	<u>0</u>	<u>0</u>								
	BUSES	<u>0</u>	<u>0</u>								
	MOTRCLS	<u>0</u>	<u>0</u>								

SPEEDS ESTIMATED BY: RADAR / DRIVING THE PACE  
 POSTED SPEED LIMIT SIGNS SAY: \_\_\_\_\_

OTHER NOISE SOURCES (BACKGROUND): DIST. AIRCRAFT RUSTLING LEAVES DIST. BARKING DOGS BIRDS DIST. INDUSTRIAL  
 DIST. KIDS PLAYING DIST. CONVRSTNS YELLING DIST. TRAFFIC (LIST RDWYS BELOW) DIST. GARDENERS/LANDSCAPING NOISE  
 OTHER: Vehicle going through Alley; Pist traffic off Santa Monica Blvd

**DESCRIPTION / SKETCH**

TERRAIN HARD SOFT MIXED FLAT OTHER: \_\_\_\_\_  
 PHOTOS See Attached  
 OTHER COMMENTS / SKETCH \_\_\_\_\_



**M6 – Commercial**

**655 N. La Peer Drive West Hollywood, California 90069**

# FIELD NOISE MEASUREMENT DATA

DUDEK

PROJECT <u>Robertson Lane</u>	PROJECT # <u>8595</u>
SITE ID <u>M6 - Commercial</u>	
SITE ADDRESS <u>655 N. La Peer Dr. West Hollywood, CA</u>	OBSERVER(S) <u>Stephanie Tang</u>
START DATE <u>2/26/15</u>	END DATE <u>2/26/15</u>
START TIME <u>10:56AM</u>	END TIME <u>11:11AM</u>

**METEOROLOGICAL CONDITIONS**

TEMP <u>69.8</u> F	HUMIDITY <u>46.5</u> % R.H.	WIND CALM <input checked="" type="radio"/> LIGHT MODERATE
WINDSPD <u>0.0</u> MPH	DIR. N NE S SE S SW W NW	VARIABLE STEADY GUSTY
SKY <u>SUNNY CLEAR</u>	OVRCAST <input type="radio"/> PRTLY CLDY <input checked="" type="radio"/> FOG	RAIN

**ACOUSTIC MEASUREMENTS**

MEAS. INSTRUMENT <u>Piccolo SLM</u>	TYPE 1 <input checked="" type="radio"/> 2	SERIAL # <u>130625008</u>
CALIBRATOR <u>BSWA CA III</u>		SERIAL # <u>49051</u>
CALIBRATION CHECK	PRE-TEST <u>94.0</u> dBA SPL	POST-TEST <u>94.0</u> dBA SPL
		WINDSCRN <input checked="" type="checkbox"/>

**SETTINGS**

A-WTT   
  SLOW   
 FAST   
 FRONTAL   
 RANDOM   
 ANSI   
 OTHER: \_\_\_\_\_

REC. #	BEGIN	END	Leq	Lmax	Lmin	L90	L50	L10	OTHER (SPECIFY METRIC)
<u>M6</u>	<u>10:56am</u>	<u>11:11AM</u>	<u>71.1</u>	<u>87.9</u>	<u>55.2</u>				

**COMMENTS**

\_\_\_\_\_

\_\_\_\_\_

**SOURCE INFO AND TRAFFIC COUNTS**

PRIMARY NOISE SOURCE  TRAFFIC    AIRCRAFT    RAIL     INDUSTRIAL    OTHER: \_\_\_\_\_

ROADWAY TYPE: N. La Peer Dr.    DIST. TO RDWY C/L OR EOP: \_\_\_\_\_

COUNT 1 (OR RDWY 1)	TRAFFIC COUNT DURATION: <u>15</u> MIN				IF COUNTING BOTH DIRECTIONS AS ONE, CHECK HERE	SPEED _____			
	DIRECTION	NB/EB	SB/WB	NB/EB		SB/WB	MIN	SB/WB	NB/EB
AUTOS	<u>18</u>	<u>5</u>							
MED TRKS	<u>0</u>	<u>0</u>							
HVY TRKS	<u>3</u>	<u>2</u>							
BUSES	<u>0</u>	<u>0</u>							
MOTRCLS	<u>0</u>	<u>0</u>							

SPEEDS ESTIMATED BY: RADAR / DRIVING THE PACE

POSTED SPEED LIMIT SIGNS SAY: 30mph

OTHER NOISE SOURCES (BACKGROUND):  DIST. AIRCRAFT     RUSTLING LEAVES     DIST. BARKING DOGS     BIRDS     DIST. INDUSTRIAL

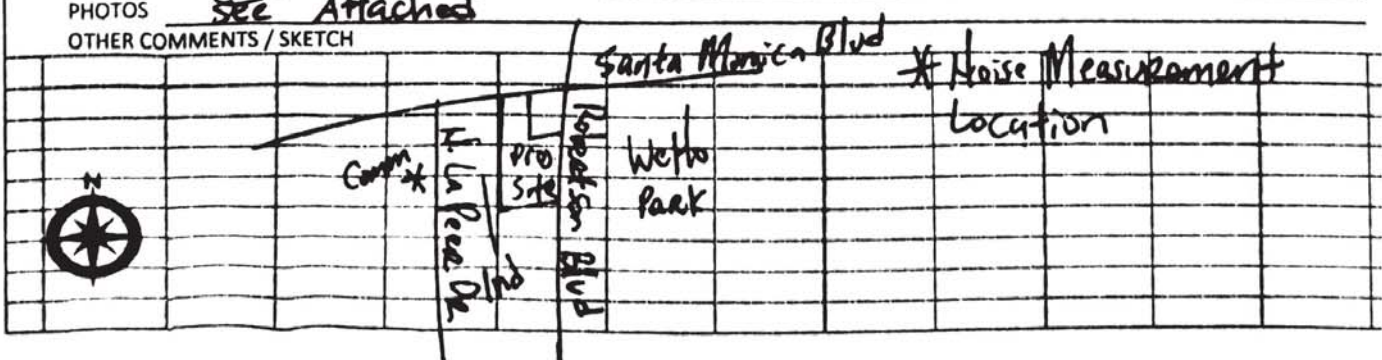
DIST. KIDS PLAYING     DIST. CONVRSTNS YELLING     DIST. TRAFFIC (LIST RDWYS BELOW)     DISTD GARDENERS/LANDSCAPING NOISE

OTHER: Industrial operation across the street; Trucks; Dist traffic off Santa Monica Blvd

**DESCRIPTION / SKETCH**

TERRAIN  HARD     SOFT     MIXED     FLAT    OTHER: \_\_\_\_\_

PHOTOS see Attached





**M7 – Commercial**

**634 N. La Peer Drive West Hollywood, California 90069**



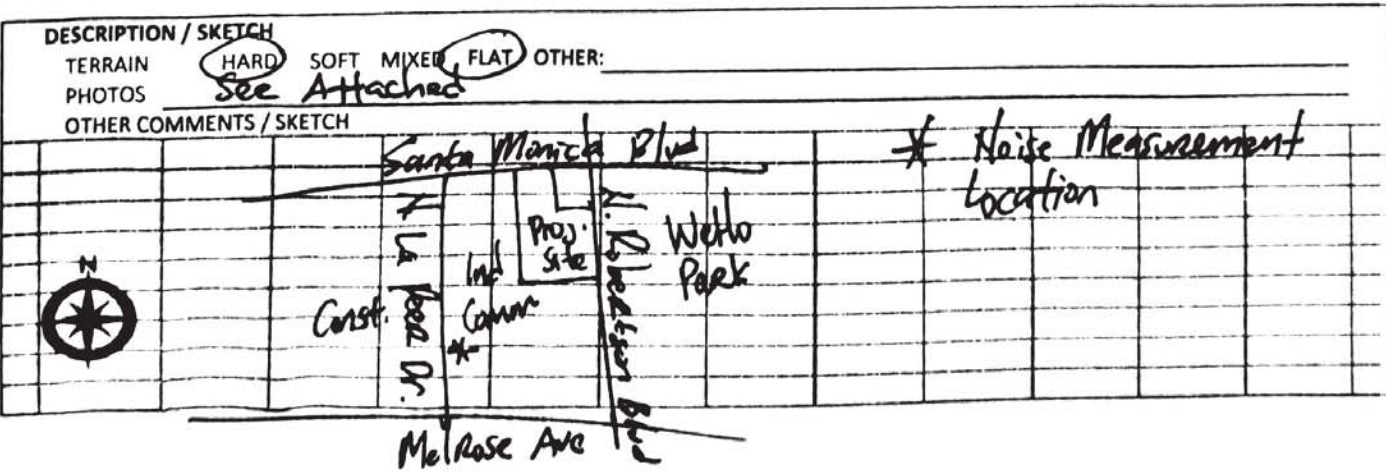
# FIELD NOISE MEASUREMENT DATA

DUDEK

PROJECT <u>Robertson Lane</u>	PROJECT # <u>8595</u>
SITE ID <u>M7 - Commercial</u>	
SITE ADDRESS <u>6311 N. La Brea Dr. West Hollywood, CA 90069</u>	OBSERVER(S) <u>Stephanie Tang</u>
START DATE <u>2/26/15</u>	END DATE <u>2/26/15</u>
START TIME <u>11:19 AM</u>	END TIME <u>11:34 AM</u>

METEOROLOGICAL CONDITIONS			
TEMP <u>71.4</u> F	HUMIDITY <u>43.8</u> % R.H.	WIND <u>CALM</u>	LIGHT MODERATE
WINDSPD <u>0</u> MPH	DIR. N NE S SE S SW W NW	VARIABLE STEADY GUSTY	
SKY <u>SUNNY</u>	CLEAR OVRCAST <u>PRTLY CLDY</u>	FOG RAIN	
ACOUSTIC MEASUREMENTS			
MEAS. INSTRUMENT <u>Piccolo SLM</u>	TYPE 1 <u>(2)</u>	SERIAL # <u>170625008</u>	
CALIBRATOR <u>Bruce CA 114</u>		SERIAL # <u>499157</u>	
CALIBRATION CHECK	PRE TEST <u>94.0</u> dBA SPL	POST-TEST <u>94.0</u> dBA SPL	WINDSCRN <u>✓</u>
SETTINGS	<u>A-WTD</u> <u>SLOW</u> FAST FRONTAL RANDOM ANSI OTHER: _____		
REC. # <u>M7</u>	BEGIN <u>11:19 AM</u>	END <u>11:34 AM</u>	Leq <u>64.9</u> Lmax <u>76.9</u> Lmin <u>58.3</u> L90 L50 L10 OTHER (SPECIFY METRIC)
COMMENTS			

SOURCE INFO AND TRAFFIC COUNTS											
PRIMARY NOISE SOURCE <u>TRAFFIC</u> AIRCRAFT RAIL INDUSTRIAL OTHER: _____											
ROADWAY TYPE: <u>N. La Brea Dr.</u> DIST. TO RDWY C/L OR EOP: <u>~20'</u>											
TRAFFIC COUNT DURATION: _____ MIN SPEED _____ MIN SPEED											
COUNT 1 (OR RDWY 1)	DIRECTION	NB/EB	SB/WB	NB/EB	SB/WB	COUNT 2 (OR RDWY 2)	NB/EB	SB/WB	NB/EB	SB/WB	
	AUTOS	<u>6</u>	<u>19</u>								
	MED TRKS	<u>1</u>	<u>3</u>								
	HVY TRKS	<u>1</u>	<u>0</u>								
	BUSES	<u>0</u>	<u>0</u>								
MOTRCLS	<u>0</u>	<u>0</u>									
SPEEDS ESTIMATED BY: RADAR / DRIVING THE PACE											
POSTED SPEED LIMIT SIGNS SAY: <u>30mph</u>											
OTHER NOISE SOURCES (BACKGROUND): <u>DIST. AIRCRAFT</u> RUSTLING LEAVES DIST. BARKING DOGS BIRDS <u>DIST. INDUSTRIAL</u>											
DIST. KIDS PLAYING <u>DIST. CONVRTNS</u> YELLING DIST. TRAFFIC (LIST RDWYS BELOW) DISTD GARDENERS/LANDSCAPING NOISE											
OTHER: <u>Const. Activity Across the Street</u>											





# FIELD NOISE MEASUREMENT DATA

DUDEK

PROJECT	Robertson Lane	PROJECT #	8595
SITE ID	MB - Residential (Back of Res)		
SITE ADDRESS	8817 Congely Ave West Hollywood, CA		
START DATE	2/26/15	END DATE	2/26/15
START TIME	12:27am	END TIME	12:42am
OBSERVER(S)	Stephanie Tang		
			90048

**METEOROLOGICAL CONDITIONS**

TEMP 73.1 F HUMIDITY 48.0 % R.H. WIND CALM LIGHT MODERATE  
 WINDSPD 1.0 MPH DIR. N NE S SE S SW W NW VARIABLE STEADY GUSTY  
 SKY SUNNY CLEAR OVRCAST PRTL CLDY FOG RAIN

**ACOUSTIC MEASUREMENTS**

MEAS. INSTRUMENT Piccolo Sum TYPE 1 2 SERIAL # 130625008  
 CALIBRATOR BSWA CA114 SERIAL # 491015  
 CALIBRATION CHECK PRE-TEST 99.0 dBA SPL POST-TEST 94.0 dBA SPL WINDSCRN

SETTINGS A-WTD SLOW FAST FRONTAL RANDOM ANSI OTHER: \_\_\_\_\_

REC. #	BEGIN	END	Leq	Lmax	Lmin	L90	L50	L10	OTHER (SPECIFY METRIC)
<u>MB</u>	<u>12:27am</u>	<u>12:42am</u>	<u>61.0</u>	<u>74.5</u>	<u>51.7</u>				

COMMENTS

**SOURCE INFO AND TRAFFIC COUNTS**

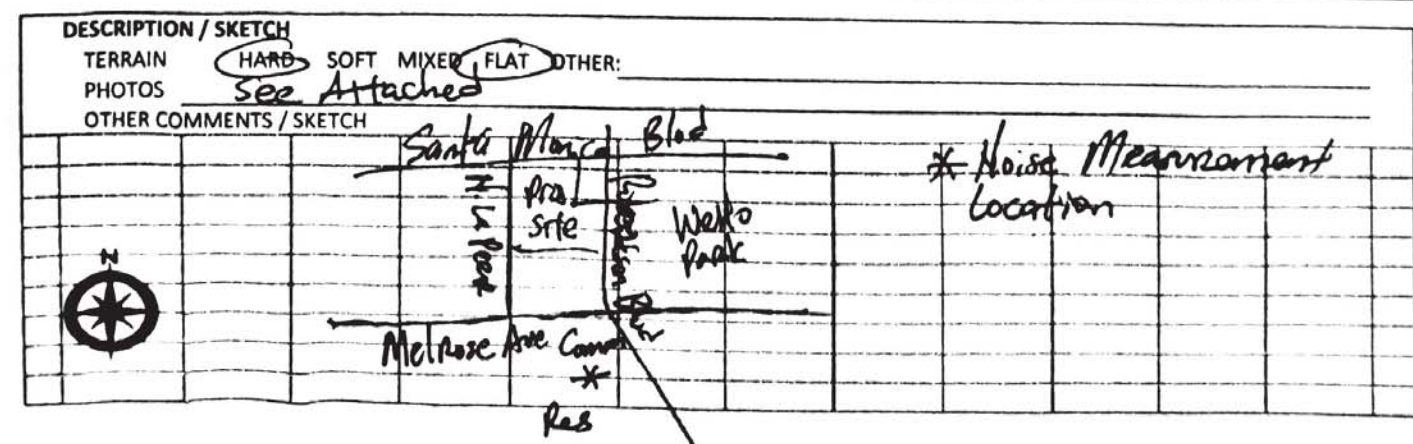
PRIMARY NOISE SOURCE TRAFFIC AIRCRAFT RAIL INDUSTRIAL OTHER: \_\_\_\_\_  
 ROADWAY TYPE: Robertson Blvd DIST. TO RDWY C/L OR EOP: ~150'

TRAFFIC COUNT DURATION: 15 MIN SPEED \_\_\_\_\_

COUNT 1 (OR RDWY 1)	DIRECTION		SPEED		IF COUNTING BOTH DIRECTIONS AS ONE, CHECK HERE	COUNT 2 (OR RDWY 2)	SPEED	
	NB/EB	SB/WB	NB/EB	SB/WB			NB/EB	SB/WB
AUTOS	<u>117</u>	<u>130</u>						
MED TRKS	<u>4</u>	<u>2</u>						
HVY TRKS	<u>0</u>	<u>0</u>						
BUSES	<u>0</u>	<u>0</u>						
MOTRCLS	<u>1</u>	<u>0</u>						

SPEEDS ESTIMATED BY: RADAR / DRIVING THE PACE  
 POSTED SPEED LIMIT SIGNS SAY: 30mph

OTHER NOISE SOURCES (BACKGROUND): TRAFFIC RUSTLING LEAVES DIST. BARKING DOGS BIRDS DIST. INDUSTRIAL  
 DIST. KIDS PLAYING DIST. CONCRETE / YELLING DIST. TRAFFIC (LIST RDWYS BELOW) DISTO GARDENERS/LANDSCAPING NOISE  
 OTHER: Vehicles driving through alley



**INPUT: ROADWAYS**

<Project Name?>

<Organization?>		14 September 2016									
<Analysis By?>		TNM 2.5									
<b>INPUT: ROADWAYS</b>							<b>Average pavement type shall be used unless a State highway agency substantiates the use of a different type with the approval of FHWA</b>				
<b>PROJECT/CONTRACT:</b>		<Project Name?>									
<b>RUN:</b>		Robertson Lane Existing + Project									
<b>Roadway Name</b>	<b>Width</b>	<b>Points Name</b>	<b>No.</b>	<b>Coordinates (pavement)</b>			<b>Flow Control</b>			<b>Segment</b>	
				<b>X</b>	<b>Y</b>	<b>Z</b>	<b>Control Device</b>	<b>Speed Constraint</b>	<b>Percent Vehicles Affected</b>	<b>Pvmt Type</b>	<b>On Struct?</b>
	ft			ft	ft	ft		mph	%		
N. San Vicente Blvd	70.0	point3	3	2,050.0	1.0	0.00				Average	
		point4	4	2,050.0	1,400.0	0.00					
N. Robertson Blvd	45.0	point11	11	1,300.0	1.0	0.00				Average	
		point35	35	1,300.0	455.5	0.00				Average	
		point12	12	1,300.0	910.0	0.00					
N. La Peer Dr	35.0	point13	13	950.0	1.0	0.00				Average	
		point14	14	950.0	670.0	0.00					
N. La Cienega Blvd	70.0	point15	15	4,050.0	-300.0	0.00				Average	
		point16	16	4,050.0	2,750.0	0.00					
Melrose Avenue	50.0	point19	19	0.0	0.0	0.00				Average	
		point20	20	4,025.0	0.0	0.00					
Santa Monica Blvd	80.0	point26	26	-185.0	-90.0	0.00				Average	
		point33	33	527.5	395.0	0.00				Average	
		point34	34	1,240.0	880.0	0.00				Average	
		point32	32	1,952.5	1,365.0	0.00				Average	
		point27	27	4,090.0	2,820.0	0.00					
Ramage Street	30.0	point28	28	820.0	640.0	0.00				Average	
		point29	29	590.0	940.0	0.00					
Almont Drive	45.0	point30	30	700.0	15.0	0.00				Average	
		point31	31	700.0	500.0	0.00					

INPUT: TRAFFIC FOR LAeq1h Volumes

<Project Name?>

<Organization?>													
<Analysis By?>													
INPUT: TRAFFIC FOR LAeq1h Volumes													
PROJECT/CONTRACT:	<Project Name?>												
RUN:	Robertson Lane Existing + Project												
Roadway	Points												
Name	Name	No.	Segment		MTrucks		HTrucks		Buses		Motorcycles		
			Autos		V	S	V	S	V	S	V	S	
			veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	
N. San Vicente Blvd	point3	3	2891	35	60	35	60	35	0	0	0	0	
	point4	4											
N. Robertson Blvd	point11	11	2075	30	43	30	43	30	0	0	0	0	
	point35	35	1251	30	26	30	26	30	0	0	0	0	
	point12	12											
N. La Peer Dr	point13	13	117	30	2	30	2	30	0	0	0	0	
	point14	14											
N. La Cienega Blvd	point15	15	0	0	0	0	0	0	0	0	0	0	
	point16	16											
Melrose Avenue	point19	19	2405	35	50	35	50	35	0	0	0	0	
	point20	20											
Santa Monica Blvd	point26	26	4326	35	90	35	90	35	0	0	0	0	
	point33	33	4197	35	87	35	87	35	0	0	0	0	
	point34	34	4501	35	94	35	94	35	0	0	0	0	
	point32	32	5191	35	108	35	108	35	0	0	0	0	
	point27	27											
Ramage Street	point28	28	24	25	8	25	0	0	0	0	0	0	
	point29	29											
Almont Drive	point30	30	284	30	6	30	6	30	0	0	0	0	
	point31	31											

**INPUT: RECEIVERS**

<Project Name?>

<Organization?>												
<Analysis By?>												
<b>INPUT: RECEIVERS</b>												
<b>PROJECT/CONTRACT:</b>	<b>&lt;Project Name?&gt;</b>											
<b>RUN:</b>	<b>Robertson Lane Existing + Project</b>											
<b>Receiver</b>												
<b>Name</b>	<b>No.</b>	<b>#DUs</b>	<b>Coordinates (ground)</b>			<b>Height</b>	<b>Input Sound Levels and Criteria</b>				<b>Active</b>	
			<b>X</b>	<b>Y</b>	<b>Z</b>	<b>above</b>	<b>Existing</b>	<b>Impact Criteria</b>		<b>NR</b>	<b>in</b>	
						<b>Ground</b>	<b>LAeq1h</b>	<b>LAeq1h</b>	<b>Sub'l</b>	<b>Goal</b>	<b>Calc.</b>	
			ft	ft	ft	ft	dBA	dBA	dB	dB		
M1	2	1	1,260.0	510.0	0.00	4.92	0.00	66	10.0	8.0	Y	
M2	3	1	1,345.0	710.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M3	5	1	1,830.0	930.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M4	7	1	1,330.0	890.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M5	9	1	675.0	750.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M6	11	1	905.0	380.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M7	13	1	975.0	270.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M8	15	1	3,885.0	-155.0	0.00	5.00	0.00	66	10.0	8.0	Y	

**RESULTS: SOUND LEVELS**

<Project Name?>

<Organization?>													14 September 2016																							
<Analysis By?>													TNM 2.5																							
													Calculated with TNM 2.5																							
<b>RESULTS: SOUND LEVELS</b>																																				
<b>PROJECT/CONTRACT:</b>													<Project Name?>																							
<b>RUN:</b>													Robertson Lane Existing + Project																							
<b>BARRIER DESIGN:</b>													INPUT HEIGHTS																							
													Average pavement type shall be used unless a State highway agency substantiates the use of a different type with approval of FHWA.																							
<b>ATMOSPHERICS:</b>													68 deg F, 50% RH																							
<b>Receiver</b>																																				
<b>Name</b>													<b>No.</b>		<b>#DUs</b>		<b>Existing</b>		<b>No Barrier</b>		<b>With Barrier</b>															
															LAeq1h		LAeq1h		Increase over existing		Type		Calculated		Noise Reduction											
																	Calculated		Crit'n		Calculated		Crit'n		Impact		LAeq1h		Calculated		Goal		Calculated			
																															minus		Goal			
															dBA		dBA		dBA		dB		dB				dBA		dB		dB		dB			
M1													2		1		0.0		67.4		66		67.4		10		Snd Lvl		67.4		0.0		8		-8.0	
M2													3		1		0.0		67.6		66		67.6		10		Snd Lvl		67.6		0.0		8		-8.0	
M3													5		1		0.0		64.9		66		64.9		10		----		64.9		0.0		8		-8.0	
M4													7		1		0.0		73.5		66		73.5		10		Snd Lvl		73.5		0.0		8		-8.0	
M5													9		1		0.0		64.2		66		64.2		10		----		64.2		0.0		8		-8.0	
M6													11		1		0.0		64.5		66		64.5		10		----		64.5		0.0		8		-8.0	
M7													13		1		0.0		63.7		66		63.7		10		----		63.7		0.0		8		-8.0	
M8													15		1		0.0		62.0		66		62.0		10		----		62.0		0.0		8		-8.0	
<b>Dwelling Units</b>															<b># DUs</b>		<b>Noise Reduction</b>																			
																	<b>Min</b>		<b>Avg</b>		<b>Max</b>															
																	dB		dB		dB															
All Selected															8		0.0		0.0		0.0															
All Impacted															3		0.0		0.0		0.0															
All that meet NR Goal															0		0.0		0.0		0.0															

**INPUT: ROADWAYS**

<Project Name?>

<Organization?>		14 September 2016									
<Analysis By?>		TNM 2.5									
<b>INPUT: ROADWAYS</b>							<b>Average pavement type shall be used unless a State highway agency substantiates the use of a different type with the approval of FHWA</b>				
<b>PROJECT/CONTRACT:</b>		<Project Name?>									
<b>RUN:</b>		Robertson Lane Existing + Project									
<b>Roadway Name</b>	<b>Width</b>	<b>Points Name</b>	<b>No.</b>	<b>Coordinates (pavement)</b>			<b>Flow Control</b>			<b>Segment</b>	
				<b>X</b>	<b>Y</b>	<b>Z</b>	<b>Control Device</b>	<b>Speed Constraint</b>	<b>Percent Vehicles Affected</b>	<b>Pvmt Type</b>	<b>On Struct?</b>
	ft			ft	ft	ft		mph	%		
N. San Vicente Blvd	70.0	point3	3	2,050.0	1.0	0.00				Average	
		point4	4	2,050.0	1,400.0	0.00					
N. Robertson Blvd	45.0	point11	11	1,300.0	1.0	0.00				Average	
		point35	35	1,300.0	455.5	0.00				Average	
		point12	12	1,300.0	910.0	0.00					
N. La Peer Dr	35.0	point13	13	950.0	1.0	0.00				Average	
		point14	14	950.0	670.0	0.00					
N. La Cienega Blvd	70.0	point15	15	4,050.0	-300.0	0.00				Average	
		point16	16	4,050.0	2,750.0	0.00					
Melrose Avenue	50.0	point19	19	0.0	0.0	0.00				Average	
		point20	20	4,025.0	0.0	0.00					
Santa Monica Blvd	80.0	point26	26	-185.0	-90.0	0.00				Average	
		point33	33	527.5	395.0	0.00				Average	
		point34	34	1,240.0	880.0	0.00				Average	
		point32	32	1,952.5	1,365.0	0.00				Average	
		point27	27	4,090.0	2,820.0	0.00					
Ramage Street	30.0	point28	28	820.0	640.0	0.00				Average	
		point29	29	590.0	940.0	0.00					
Almont Drive	45.0	point30	30	700.0	15.0	0.00				Average	
		point31	31	700.0	500.0	0.00					



**INPUT: TRAFFIC FOR LAeq1h Volumes**

<Project Name?>

<Organization?>													
<Analysis By?>													
<b>INPUT: TRAFFIC FOR LAeq1h Volumes</b>													
<b>PROJECT/CONTRACT:</b>	<Project Name?>												
<b>RUN:</b>	Robertson Lane Existing + Project												
<b>Roadway</b>	<b>Points</b>												
<b>Name</b>	<b>Name</b>	<b>No.</b>	<b>Segment</b>		<b>MTrucks</b>		<b>HTrucks</b>		<b>Buses</b>		<b>Motorcycles</b>		
			<b>Autos</b>		<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	
			<b>veh/hr</b>	<b>mph</b>	<b>veh/hr</b>	<b>mph</b>	<b>veh/hr</b>	<b>mph</b>	<b>veh/hr</b>	<b>mph</b>	<b>veh/hr</b>	<b>mph</b>	
N. San Vicente Blvd	point3	3	2944	35	61	35	61	35	0	0	0	0	
	point4	4											
N. Robertson Blvd	point11	11	2153	30	45	30	45	30	0	0	0	0	
	point35	35	1358	30	28	30	28	30	0	0	0	0	
	point12	12											
N. La Peer Dr	point13	13	165	30	3	30	3	30	0	0	0	0	
	point14	14											
N. La Cienega Blvd	point15	15	0	0	0	0	0	0	0	0	0	0	
	point16	16											
Melrose Avenue	point19	19	2466	35	51	35	51	35	0	0	0	0	
	point20	20											
Santa Monica Blvd	point26	26	4514	35	94	35	94	35	0	0	0	0	
	point33	33	4364	35	91	35	91	35	0	0	0	0	
	point34	34	4628	35	96	35	96	35	0	0	0	0	
	point32	32	5314	35	111	35	111	35	0	0	0	0	
	point27	27											
Ramage Street	point28	28	24	25	8	25	0	0	0	0	0	0	
	point29	29											
Almont Drive	point30	30	284	30	6	30	6	30	0	0	0	0	
	point31	31											

**INPUT: RECEIVERS**

<Project Name?>

<Organization?>												
<Analysis By?>												
<b>INPUT: RECEIVERS</b>												
<b>PROJECT/CONTRACT:</b>	<b>&lt;Project Name?&gt;</b>											
<b>RUN:</b>	<b>Robertson Lane Existing + Project</b>											
<b>Receiver</b>												
<b>Name</b>	<b>No.</b>	<b>#DUs</b>	<b>Coordinates (ground)</b>			<b>Height</b>	<b>Input Sound Levels and Criteria</b>				<b>Active</b>	
			<b>X</b>	<b>Y</b>	<b>Z</b>	<b>above</b>	<b>Existing</b>	<b>Impact Criteria</b>		<b>NR</b>	<b>in</b>	
						<b>Ground</b>	<b>LAeq1h</b>	<b>LAeq1h</b>	<b>Sub'l</b>	<b>Goal</b>	<b>Calc.</b>	
			ft	ft	ft	ft	dBA	dBA	dB	dB		
M1	2	1	1,260.0	510.0	0.00	4.92	0.00	66	10.0	8.0	Y	
M2	3	1	1,345.0	710.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M3	5	1	1,830.0	930.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M4	7	1	1,330.0	890.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M5	9	1	675.0	750.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M6	11	1	905.0	380.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M7	13	1	975.0	270.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M8	15	1	3,885.0	-155.0	0.00	5.00	0.00	66	10.0	8.0	Y	

**RESULTS: SOUND LEVELS**

<Project Name?>

<Organization?>													14 September 2016																							
<Analysis By?>													TNM 2.5																							
													Calculated with TNM 2.5																							
<b>RESULTS: SOUND LEVELS</b>																																				
<b>PROJECT/CONTRACT:</b>													<Project Name?>																							
<b>RUN:</b>													Robertson Lane Existing + Project																							
<b>BARRIER DESIGN:</b>													INPUT HEIGHTS																							
													Average pavement type shall be used unless a State highway agency substantiates the use of a different type with approval of FHWA.																							
<b>ATMOSPHERICS:</b>													68 deg F, 50% RH																							
<b>Receiver</b>																																				
<b>Name</b>													<b>No.</b>		<b>#DUs</b>		<b>Existing</b>		<b>No Barrier</b>		<b>With Barrier</b>															
															LAeq1h		LAeq1h		Increase over existing		Type		Calculated		Noise Reduction											
																	Calculated		Crit'n		Calculated		Crit'n		Impact		LAeq1h		Calculated		Goal		Calculated			
																															minus		Goal			
															dBA		dBA		dBA		dB		dB				dBA		dB		dB		dB			
M1													2		1		0.0		67.6		66		67.6		10		Snd Lvl		67.6		0.0		8		-8.0	
M2													3		1		0.0		67.8		66		67.8		10		Snd Lvl		67.8		0.0		8		-8.0	
M3													5		1		0.0		65.0		66		65.0		10		----		65.0		0.0		8		-8.0	
M4													7		1		0.0		73.6		66		73.6		10		Snd Lvl		73.6		0.0		8		-8.0	
M5													9		1		0.0		64.3		66		64.3		10		----		64.3		0.0		8		-8.0	
M6													11		1		0.0		64.8		66		64.8		10		----		64.8		0.0		8		-8.0	
M7													13		1		0.0		64.2		66		64.2		10		----		64.2		0.0		8		-8.0	
M8													15		1		0.0		62.1		66		62.1		10		----		62.1		0.0		8		-8.0	
<b>Dwelling Units</b>															<b># DUs</b>		<b>Noise Reduction</b>																			
																	<b>Min</b>		<b>Avg</b>		<b>Max</b>															
																	dB		dB		dB															
All Selected															8		0.0		0.0		0.0															
All Impacted															3		0.0		0.0		0.0															
All that meet NR Goal															0		0.0		0.0		0.0															

**INPUT: ROADWAYS**

<Project Name?>

<Organization?>		14 September 2016									
<Analysis By?>		TNM 2.5									
<b>INPUT: ROADWAYS</b>		<Project Name?>					Average pavement type shall be used unless a State highway agency substantiates the use of a different type with the approval of FHWA				
<b>PROJECT/CONTRACT:</b>		Robertson Lane Future Without Project									
<b>RUN:</b>		Robertson Lane Future Without Project									
Roadway Name	Width	Points		Coordinates (pavement)			Flow Control			Segment	On Struct?
		Name	No.	X	Y	Z	Control Device	Speed Constraint	Percent Vehicles Affected		
	ft			ft	ft	ft		mph	%		
N. San Vicente Blvd	70.0	point3	3	2,050.0	1.0	0.00				Average	
		point4	4	2,050.0	1,400.0	0.00					
N. Robertson Blvd	45.0	point11	11	1,300.0	1.0	0.00				Average	
		point35	35	1,300.0	455.5	0.00				Average	
		point12	12	1,300.0	910.0	0.00					
N. La Peer Dr	35.0	point13	13	950.0	1.0	0.00				Average	
		point14	14	950.0	670.0	0.00					
N. La Cienega Blvd	70.0	point15	15	4,050.0	-300.0	0.00				Average	
		point16	16	4,050.0	2,750.0	0.00					
Melrose Avenue	50.0	point19	19	0.0	0.0	0.00				Average	
		point20	20	4,025.0	0.0	0.00					
Santa Monica Blvd	80.0	point26	26	-185.0	-90.0	0.00				Average	
		point33	33	527.5	395.0	0.00				Average	
		point34	34	1,240.0	880.0	0.00				Average	
		point32	32	1,952.5	1,365.0	0.00				Average	
		point27	27	4,090.0	2,820.0	0.00					
Ramage Street	30.0	point28	28	820.0	640.0	0.00				Average	
		point29	29	590.0	940.0	0.00					
Almont Drive	45.0	point30	30	700.0	15.0	0.00				Average	
		point31	31	700.0	500.0	0.00					

**INPUT: TRAFFIC FOR LAeq1h Volumes**

<Project Name?>

<Organization?>													
<Analysis By?>													
<b>INPUT: TRAFFIC FOR LAeq1h Volumes</b>													
<b>PROJECT/CONTRACT:</b>	<Project Name?>												
<b>RUN:</b>	Robertson Lane Future Without Project												
<b>Roadway</b>	<b>Points</b>												
<b>Name</b>	<b>Name</b>	<b>No.</b>	<b>Segment</b>		<b>MTrucks</b>		<b>HTrucks</b>		<b>Buses</b>		<b>Motorcycles</b>		
			<b>Autos</b>		<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	
			<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	
			veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	
N. San Vicente Blvd	point3	3	3639	35	76	35	76	35	0	0	0	0	
	point4	4											
N. Robertson Blvd	point11	11	2442	30	51	30	51	30	0	0	0	0	
	point35	35	1377	30	29	30	29	30	0	0	0	0	
	point12	12											
N. La Peer Dr	point13	13	122	30	3	30	3	30	0	0	0	0	
	point14	14											
N. La Cienega Blvd	point15	15	0	0	0	0	0	0	0	0	0	0	
	point16	16											
Melrose Avenue	point19	19	2746	35	57	35	57	35	0	0	0	0	
	point20	20											
Santa Monica Blvd	point26	26	524	35	109	35	109	35	0	0	0	0	
	point33	33	5196	35	108	35	108	35	0	0	0	0	
	point34	34	5562	35	116	35	116	35	0	0	0	0	
	point32	32	6277	35	131	35	131	35	0	0	0	0	
	point27	27											
Ramage Street	point28	28	24	25	8	25	0	0	0	0	0	0	
	point29	29											
Almont Drive	point30	30	385	30	8	30	8	30	0	0	0	0	
	point31	31											

**INPUT: RECEIVERS**

<Project Name?>

<Organization?>												
<Analysis By?>												
							14 September 2016					
							TNM 2.5					
<b>INPUT: RECEIVERS</b>												
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<b>RUN:</b>		Robertson Lane Future Without Project										
<b>Receiver</b>												
<b>Name</b>	<b>No.</b>	<b>#DUs</b>	<b>Coordinates (ground)</b>			<b>Height</b>	<b>Input Sound Levels and Criteria</b>				<b>Active</b>	
			<b>X</b>	<b>Y</b>	<b>Z</b>	<b>above</b>	<b>Existing</b>	<b>Impact Criteria</b>		<b>NR</b>	<b>in</b>	
						<b>Ground</b>	<b>LAeq1h</b>	<b>LAeq1h</b>	<b>Sub'l</b>	<b>Goal</b>	<b>Calc.</b>	
			ft	ft	ft	ft	dBA	dBA	dB	dB		
M1	2	1	1,260.0	510.0	0.00	4.92	0.00	66	10.0	8.0	Y	
M2	3	1	1,345.0	710.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M3	5	1	1,830.0	930.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M4	7	1	1,330.0	890.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M5	9	1	675.0	750.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M6	11	1	905.0	380.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M7	13	1	975.0	270.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M8	15	1	3,885.0	-155.0	0.00	5.00	0.00	66	10.0	8.0	Y	

**RESULTS: SOUND LEVELS**

<Project Name?>

<Organization?>													14 September 2016																							
<Analysis By?>													TNM 2.5																							
													Calculated with TNM 2.5																							
<b>RESULTS: SOUND LEVELS</b>																																				
<b>PROJECT/CONTRACT:</b>													<Project Name?>																							
<b>RUN:</b>													Robertson Lane Future Without Project																							
<b>BARRIER DESIGN:</b>													INPUT HEIGHTS																							
													Average pavement type shall be used unless a State highway agency substantiates the use of a different type with approval of FHWA.																							
<b>ATMOSPHERICS:</b>													68 deg F, 50% RH																							
<b>Receiver</b>																																				
<b>Name</b>													<b>No.</b>		<b>#DUs</b>		<b>Existing</b>		<b>No Barrier</b>		<b>With Barrier</b>															
															<b>L<sub>Aeq1h</sub></b>		<b>L<sub>Aeq1h</sub></b>		<b>Increase over existing</b>		<b>Type</b>		<b>Calculated</b>		<b>Noise Reduction</b>											
																	<b>Calculated</b>		<b>Crit'n</b>		<b>Calculated</b>		<b>Crit'n</b>		<b>Impact</b>		<b>L<sub>Aeq1h</sub></b>		<b>Calculated</b>		<b>Goal</b>		<b>Calculated</b>			
																															<b>minus</b>		<b>Goal</b>			
															dBA		dBA		dBA		dB		dB				dBA		dB		dB		dB			
M1													2		1		0.0		67.9		66		67.9		10		Snd Lvl		67.9		0.0		8		-8.0	
M2													3		1		0.0		68.3		66		68.3		10		Snd Lvl		68.3		0.0		8		-8.0	
M3													5		1		0.0		65.9		66		65.9		10		----		65.9		0.0		8		-8.0	
M4													7		1		0.0		74.3		66		74.3		10		Snd Lvl		74.3		0.0		8		-8.0	
M5													9		1		0.0		64.7		66		64.7		10		----		64.7		0.0		8		-8.0	
M6													11		1		0.0		65.1		66		65.1		10		----		65.1		0.0		8		-8.0	
M7													13		1		0.0		64.3		66		64.3		10		----		64.3		0.0		8		-8.0	
M8													15		1		0.0		62.6		66		62.6		10		----		62.6		0.0		8		-8.0	
<b>Dwelling Units</b>															<b># DUs</b>		<b>Noise Reduction</b>																			
																	<b>Min</b>		<b>Avg</b>		<b>Max</b>															
																	dB		dB		dB															
All Selected															8		0.0		0.0		0.0															
All Impacted															3		0.0		0.0		0.0															
All that meet NR Goal															0		0.0		0.0		0.0															

**INPUT: ROADWAYS**

<Project Name?>

<Organization?>		14 September 2016									
<Analysis By?>		TNM 2.5									
<b>INPUT: ROADWAYS</b>		<Project Name?>					Average pavement type shall be used unless a State highway agency substantiates the use of a different type with the approval of FHWA				
<b>PROJECT/CONTRACT:</b>		Robertson Lane Future With Project									
<b>RUN:</b>		Robertson Lane Future With Project									
Roadway Name	Width	Points		Coordinates (pavement)			Flow Control			Segment	On Struct?
		Name	No.	X	Y	Z	Control Device	Speed Constraint	Percent Vehicles Affected		
	ft			ft	ft	ft		mph	%		
N. San Vicente Blvd	70.0	point3	3	2,050.0	1.0	0.00				Average	
		point4	4	2,050.0	1,400.0	0.00					
N. Robertson Blvd	45.0	point11	11	1,300.0	1.0	0.00				Average	
		point35	35	1,300.0	455.5	0.00				Average	
		point12	12	1,300.0	910.0	0.00					
N. La Peer Dr	35.0	point13	13	950.0	1.0	0.00				Average	
		point14	14	950.0	670.0	0.00					
N. La Cienega Blvd	70.0	point15	15	4,050.0	-300.0	0.00				Average	
		point16	16	4,050.0	2,750.0	0.00					
Melrose Avenue	50.0	point19	19	0.0	0.0	0.00				Average	
		point20	20	4,025.0	0.0	0.00					
Santa Monica Blvd	80.0	point26	26	-185.0	-90.0	0.00				Average	
		point33	33	527.5	395.0	0.00				Average	
		point34	34	1,240.0	880.0	0.00				Average	
		point32	32	1,952.5	1,365.0	0.00				Average	
		point27	27	4,090.0	2,820.0	0.00					
Ramage Street	30.0	point28	28	820.0	640.0	0.00				Average	
		point29	29	590.0	940.0	0.00					
Almont Drive	45.0	point30	30	700.0	15.0	0.00				Average	
		point31	31	700.0	500.0	0.00					



**INPUT: TRAFFIC FOR LAeq1h Volumes**

<Project Name?>

<Organization?>													
<Analysis By?>													
				14 September 2016									
				TNM 2.5									
<b>INPUT: TRAFFIC FOR LAeq1h Volumes</b>													
<b>PROJECT/CONTRACT:</b>		<Project Name?>											
<b>RUN:</b>		Robertson Lane Future With Project											
<b>Roadway</b>	<b>Points</b>												
<b>Name</b>	<b>Name</b>	<b>No.</b>	<b>Segment</b>		<b>MTrucks</b>		<b>HTrucks</b>		<b>Buses</b>		<b>Motorcycles</b>		
			<b>Autos</b>		<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	<b>V</b>	<b>S</b>	
			veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	veh/hr	mph	
N. San Vicente Blvd	point3	3	3659	35	76	35	76	35	0	0	0	0	
	point4	4											
N. Robertson Blvd	point11	11	2523	30	53	30	53	30	0	0	0	0	
	point35	35	1484	30	31	30	31	30	0	0	0	0	
	point12	12											
N. La Peer Dr	point13	13	170	30	4	30	4	30	0	0	0	0	
	point14	14											
N. La Cienega Blvd	point15	15	0	0	0	0	0	0	0	0	0	0	
	point16	16											
Melrose Avenue	point19	19	2807	35	58	35	58	35	0	0	0	0	
	point20	20											
Santa Monica Blvd	point26	26	5440	35	113	35	113	35	0	0	0	0	
	point33	33	4980	35	104	35	104	35	0	0	0	0	
	point34	34	5689	35	119	35	119	35	0	0	0	0	
	point32	32	6368	35	133	35	133	35	0	0	0	0	
	point27	27											
Ramage Street	point28	28	24	25	8	25	0	0	0	0	0	0	
	point29	29											
Almont Drive	point30	30	385	30	8	30	8	30	0	0	0	0	
	point31	31											

**INPUT: RECEIVERS**

<Project Name?>

<Organization?>												
<Analysis By?>												
							14 September 2016					
							TNM 2.5					
<b>INPUT: RECEIVERS</b>												
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<b>RUN:</b>		Robertson Lane Future With Project										
<b>Receiver</b>												
<b>Name</b>	<b>No.</b>	<b>#DUs</b>	<b>Coordinates (ground)</b>			<b>Height</b>	<b>Input Sound Levels and Criteria</b>				<b>Active</b>	
			<b>X</b>	<b>Y</b>	<b>Z</b>	<b>above</b>	<b>Existing</b>	<b>Impact Criteria</b>		<b>NR</b>	<b>in</b>	
						<b>Ground</b>	<b>LAeq1h</b>	<b>LAeq1h</b>	<b>Sub'l</b>	<b>Goal</b>	<b>Calc.</b>	
			ft	ft	ft	ft	dBA	dBA	dB	dB		
M1	2	1	1,260.0	510.0	0.00	4.92	0.00	66	10.0	8.0	Y	
M2	3	1	1,345.0	710.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M3	5	1	1,830.0	930.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M4	7	1	1,330.0	890.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M5	9	1	675.0	750.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M6	11	1	905.0	380.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M7	13	1	975.0	270.0	0.00	5.00	0.00	66	10.0	8.0	Y	
M8	15	1	3,885.0	-155.0	0.00	5.00	0.00	66	10.0	8.0	Y	

**RESULTS: SOUND LEVELS**

<Project Name?>

<Organization?>		14 September 2016										
<Analysis By?>		TNM 2.5										
		Calculated with TNM 2.5										
<b>RESULTS: SOUND LEVELS</b>												
<b>PROJECT/CONTRACT:</b>		<Project Name?>										
<b>RUN:</b>		Robertson Lane Future With Project										
<b>BARRIER DESIGN:</b>		INPUT HEIGHTS										
		Average pavement type shall be used unless a State highway agency substantiates the use of a different type with approval of FHWA.										
<b>ATMOSPHERICS:</b>		68 deg F, 50% RH										
<b>Receiver</b>												
<b>Name</b>	<b>No.</b>	<b>#DUs</b>	<b>Existing LAeq1h</b>	<b>No Barrier LAeq1h</b>	<b>Increase over existing</b>		<b>Type</b>	<b>With Barrier</b>	<b>Noise Reduction</b>			
				<b>Calculated</b>	<b>Crit'n</b>	<b>Calculated</b>	<b>Crit'n</b>	<b>Impact</b>	<b>Calculated LAeq1h</b>	<b>Calculated</b>	<b>Goal</b>	<b>Calculated minus Goal</b>
			<b>dBA</b>	<b>dBA</b>	<b>dBA</b>	<b>dB</b>	<b>dB</b>		<b>dBA</b>	<b>dB</b>	<b>dB</b>	<b>dB</b>
M1	2	1	0.0	68.2	66	68.2	10	Snd Lvl	68.2	0.0	8	-8.0
M2	3	1	0.0	68.4	66	68.4	10	Snd Lvl	68.4	0.0	8	-8.0
M3	5	1	0.0	65.9	66	65.9	10	----	65.9	0.0	8	-8.0
M4	7	1	0.0	74.4	66	74.4	10	Snd Lvl	74.4	0.0	8	-8.0
M5	9	1	0.0	64.9	66	64.9	10	----	64.9	0.0	8	-8.0
M6	11	1	0.0	65.4	66	65.4	10	----	65.4	0.0	8	-8.0
M7	13	1	0.0	64.9	66	64.9	10	----	64.9	0.0	8	-8.0
M8	15	1	0.0	62.7	66	62.7	10	----	62.7	0.0	8	-8.0
<b>Dwelling Units</b>		<b># DUs</b>	<b>Noise Reduction</b>									
			<b>Min</b>	<b>Avg</b>	<b>Max</b>							
			<b>dB</b>	<b>dB</b>	<b>dB</b>							
All Selected		8	0.0	0.0	0.0							
All Impacted		3	0.0	0.0	0.0							
All that meet NR Goal		0	0.0	0.0	0.0							

Noise Impact Study

**ROBERTSON LANE HOTEL PROJECT  
WEST HOLLYWOOD, CALIFORNIA**

*Prepared for:*  
City of West Hollywood  
Community Development Department

June 2016

*Report Ref:*  
R2014115.3

*Prepared by:*  
Acoustical Engineering Services, Inc.  
22801 Crespi Street  
Woodland Hills, CA 91364

## Table of Content

Executive summary.....		3
1	Introduction.....	5
	1.1 Purpose .....	5
2	Environmental Setting .....	7
	2.1 Fundamentals of Sound and Environmental Noise .....	7
	2.1.1 Outdoor Sound Propagation.....	7
	2.1.2 Environmental Noise Descriptors .....	8
	2.2 Regulatory Framework .....	9
	2.2.1 City of West Hollywood General Plan .....	10
	2.2.2 City of West Hollywood Noise Control Ordinance .....	11
	2.3 Existing Ambient Noise Levels.....	12
3	Impact Analysis .....	16
	3.1 Thresholds of Significance .....	16
	3.2 Operation Impacts .....	18
4	Project design features .....	21

## List of Figures

Figure 1. Project Site Map.....	6
Figure 2. Noise Measurement Locations.....	14

## List of Tables

Table 1. Typical Noise Levels.....	8
Table 2. City of West Hollywood Guidelines for Noise Compatible Land Use .....	12
Table 3. Description of Noise Measurement Locations .....	15
Table 4. Existing Ambient Noise Levels.....	15
Table 5. Outdoor Use Assumptions.....	19
Table 6. Outdoor Uses Noise Levels – Daytime Hours (8 a.m. to 10 p.m.).....	19
Table 7. Outdoor Uses Noise Levels – Nighttime Hours (10 p.m. to 8 a.m.) .....	20

## Appendices

- Appendix A – Ambient Noise Measurements Data
- Appendix B – Noise Calculations

## EXECUTIVE SUMMARY

In response to a request from the City of West Hollywood, Acoustical Engineering Services, Inc. (AES) has conducted this Noise Impact Study (Study) to analyze the potential noise impacts that would result from the outdoor uses associated with the proposed Robertson Lane Hotel in the City of West Hollywood, California (Project), as shown in Figure 1 (on page 6).

The current ambient noise levels at the sensitive noise receptors (e.g., residential and park) in the vicinity of the Project Site were measured and tabulated in this report. The measured ambient sound data were utilized as baseline levels in conjunction with the City of West Hollywood noise standards and guidelines, to define the Project's noise impact thresholds. In general, the existing sound environment in the vicinity of the Project Site is dominated by local auto traffic (e.g., Santa Monica Boulevard and Robertson Boulevard) and nearby commercial uses (e.g., retail uses and restaurants).

Potential noise impacts from the Project's outdoor uses (due to people gathering and the use of amplified sound systems) at the Project's Levels 1, 3, 4 and 9 were evaluated at the off-site noise sensitive uses. To represent a conservative noise scenario, the noise levels were calculated based on the assumption of concurrent use of all the outdoor areas with the maximum number of people as well as simultaneous use of amplified sound. The key findings of the noise analysis are as follows:

- The estimated noise levels from the people gathering (e.g., talking/conversing) at the Project's proposed outdoor uses would be below the applicable significance threshold for both daytime and nighttime hours.
- The Project's amplified sound system at the Levels 1, 3 and 4 outdoor areas (i.e., outdoor dining, terrace, and pool area) would be employed primarily to broadcast background music. The amplified sound system would be designed to a maximum 75 dBA ( $L_{eq}$ ) sound level (during daytime hours from 8:00 a.m. to 10:00 p.m.) and 55 to 65 dBA ( $L_{eq}$ ) sound level (during nighttime hours from 10:00 p.m. to 8:00 a.m.). The estimated noise levels from the Levels 1, 3 and 4 amplified sound system to the off-site noise sensitive receptors would be below the applicable significance threshold for both daytime and nighttime hours.
- The Project's amplified sound system at the Level 9 outdoor areas would be used in connection with the Hotel for scheduled banquets and parties. During daytime hours from 8:00 a.m. to 10:00 p.m. the sound level output for the outdoor amplified sound system at Level 9 would be higher than Levels 1, 3, and 4, at approximately 85 dBA ( $L_{eq}$ ). Based on the maximum 85 dBA amplified sound level, the Project sound system sound output would be below the applicable daytime significance threshold at the off-site sensitive receptors. During nighttime hours from 10:00 p.m. to 8:00 a.m. the

amplified sound system would be designed to a maximum of 65 dBA ( $L_{eq}$ ). The estimated noise levels from the Level 9 amplified sound system to the off-site noise sensitive receptors would be below the applicable significance threshold for nighttime hours.

- The cumulative noise levels from use of the outdoor areas on Levels 1, 3, 4 and 9 (including both people gathering and the use of amplified sound system) would be below the applicable significance threshold for both daytime and nighttime hours.

# 1 INTRODUCTION

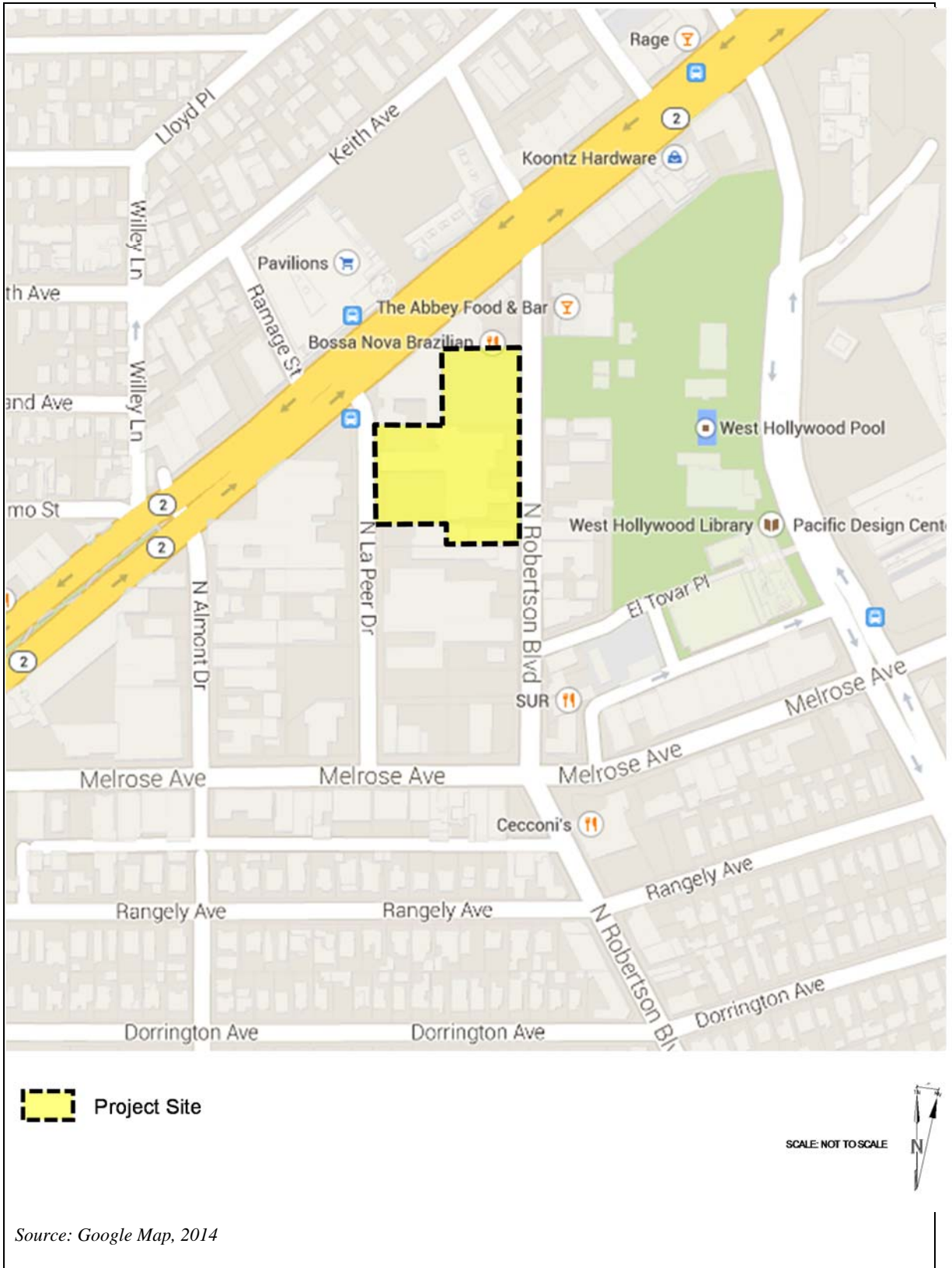
The proposed Robertson Lane Hotel Project includes several outdoor uses which would operate from 7 a.m. to 2 a.m. The outdoor uses, dining and meeting areas, located on the Hotel building Levels 1, 3, 4 and 9 will incorporate amplified sound systems to enhance/ broadcast and reinforce background music and spoken words. This study evaluates the potential noise impacts from the Project's outdoor uses on existing off-site sensitive land uses and develops noise Project Design Features, as required.

## 1.1 Purpose

The objectives of this noise study are to:

- a) Determine potential noise impacts on noise sensitive uses from Project operation-related outdoor uses, including people gathering and amplified sound systems, and
- b) Provide Project Design Features to avoid or reduce the potential noise impacts.





**Figure 1. Project Site Map**

## 2 ENVIRONMENTAL SETTING

### 2.1 Fundamentals of Sound and Environmental Noise

Noise is commonly defined as sound that is undesirable because it can interfere with speech communication and hearing, may cause sleep disturbance, or may otherwise be considered annoying (unwanted sound). The decibel (dB) is a conventional unit for measuring the amplitude of sound because it accounts for the large variations in sound pressure amplitude and reflects the way people perceive changes in sound amplitude.<sup>1</sup> The human hearing system is not equally sensitive to sound at all frequencies. Therefore, to approximate this human frequency-dependent response, the A-weighted filtering system is used to adjust measured sound levels (dBA). The term “A-weighted” refers to filtering the noise signal in a manner that corresponds to the way the human ear perceives sound. Examples of various sound levels in different environments are provided in Table 1 (on page 8).

Generally, people judge the relative magnitude of sound sensation by subjective terms such as “loudness” or “noisiness.” To the normal human ear, a change in sound level of 3 dB is considered “just perceptible,” a change in sound level of 5 dB is considered “clearly noticeable,” and a change (i.e., increase) of 10 dB is generally recognized as “twice as loud.”<sup>2</sup>

#### 2.1.1 Outdoor Sound Propagation

In an outdoor environment, sound levels attenuate (reduce) through the air as a function of distance. Such attenuation is commonly referred to as “distance loss” or “geometric spreading,” and is based on the noise source configuration (e.g., point source, or line source). For a point source, such as electronic speaker systems and outdoor gatherings, the rate of sound attenuation is about 6 dB per doubling of distance from the noise source. For example, an outdoor speaker system generates a sound level of 60 dBA at a distance of five feet would attenuate to 54 dBA at a distance of 10 feet. For a line source, such as a constant flow of traffic on a roadway, the rate of sound attenuation is about 3 dB per doubling of distance.<sup>3</sup>

In addition, structures (e.g., buildings, parapet walls) and natural topography (e.g., hills) that obstruct the line-of-sight between a noise source and a receptor further reduce the noise level if the receptor is located within the “shadow” of the obstruction, such as behind a sound wall. This type of sound attenuation is known as “barrier insertion loss.” If a receptor is located behind the wall but still has a view of the source (i.e., line-of-sight is not fully blocked), some barrier insertion loss would still occur, however to a lesser extent. Additionally, a receptor located on the same side of the wall as a noise source may actually experience an increase in the perceived noise level as the wall reflects noise back to the receptor, thereby compounding

---

<sup>1</sup> All sound levels measured in decibel (dB) in this study are relative to  $2 \times 10^{-5} \text{ N/m}^2$ .

<sup>2</sup> *Engineering Noise Control*, Bies & Hansen, 1988.

<sup>3</sup> Caltrans, “*Technical Noise Supplement (TeNS)*”, 2009.

the noise. Outdoor noise barriers can provide noise level reductions ranging from approximately 5 dBA (where the barrier just breaks the line-of-sight between the noise source and receiver) to an upper range of 20 dBA with a more substantial barrier.<sup>4</sup>

**Table 1. Typical Noise Levels**

Common Outdoor Activities	Noise Levels, dBA	Common Indoor Activities
	<b>110</b>	Rock Band
Jet Fly-over at 1000 feet		
	<b>100</b>	
Gas Lawn Mower at 3 feet		
	<b>90</b>	
Diesel Truck at 50 feet at 50 mph		Food Blender at 3 feet
	<b>80</b>	Garbage Disposal at 3 feet
Noisy Urban Area, Daytime		
Gas Lawn Mower at 100 feet	<b>70</b>	Vacuum Cleaner at 10 feet
Commercial Area		Normal Speech at 3 feet
Heavy Traffic at 300 feet	<b>60</b>	
		Large Business Office
Quiet Urban Daytime	<b>50</b>	Dishwasher Next Room
Quiet Urban Nighttime	<b>40</b>	Theater, Large Conference Room (background)
Quiet Suburban Nighttime		
	<b>30</b>	Library
Quiet Rural Nighttime		Bedroom at Night, Concert Hall (background)
	<b>20</b>	
		Broadcast/Recording Studio (background)
	<b>10</b>	
Lowest Threshold of Human Hearing	<b>0</b>	Lowest Threshold of Human Hearing

*Source: Caltrans, Technical Noise Supplement (TeNS), 2009*

### 2.1.2 Environmental Noise Descriptors

Several rating scales have been developed to analyze the adverse effect of community noise on people. Since environmental noise fluctuates over time, these scales consider the total acoustical energy content, as well as the time and duration of occurrence. The most frequently used noise descriptors, including those used by the City of West Hollywood, are summarized below.

<sup>4</sup> Caltrans, "Technical Noise Supplement (TeNS)", 2009.

*Equivalent Sound Level ( $L_{eq}$ ).*  $L_{eq}$  is a measurement of the acoustic energy content of noise averaged over a specified time period. Thus, the  $L_{eq}$  of a time-varying sound and that of a steady sound are the same if they deliver the same amount of energy to the receptor's ear during exposure.  $L_{eq}$  for one-hour periods, during the daytime or nighttime hours, and 24 hours are commonly used in environmental noise assessments.  $L_{eq}$  can be measured for any time period, but is typically measured for an increment of no less than 15 minutes for environmental studies. For evaluating community impacts, this rating scale does not vary, regardless of whether the noise occurs during day or night.

*Statistical Sound Level ( $L_n$ ).*  $L_n$  is a statistical description of the sound level that is exceeded over some fraction of a given period of time. For example, the  $L_{50}$  noise level represents the noise level that is exceeded 50 percent of the time. Half the time the noise level exceeds this level and half the time the noise level is less than this level.  $L_{90}$  noise level represents the noise level that is exceeded 90 percent of the time and for environmental noise is representative of background ambient noise level.

*Community Noise Equivalent Level (CNEL).* CNEL is the time average of all A-weighted sound levels for a 24-hour period with a 10 dBA adjustment (upward) added to the sound levels that occur between the hours of 10:00 P.M. and 7:00 A.M. (nighttime), and a 5 dBA adjustment (upward) added to the sound levels which occur between the hours of 7:00 P.M. and 10:00 P.M. (evening). These penalties attempt to account for increased human sensitivity to noise during the nighttime and evening periods, particularly where sleep is the most probable activity. CNEL has been adopted by the State of California to define the community noise environment for development of the community noise element of a General Plan and is also used by the City of West Hollywood for land use planning in the City's General Plan.<sup>5</sup>

*Day/Night Average Sound Level ( $L_{dn}$ ).*  $L_{dn}$  is the time average of all A-weighted sound levels for a 24-hour period, similar to the CNEL.  $L_{dn}$  includes a 10 dBA adjustment (upward) added to the sound levels that occur between the hours of 10:00 P.M. and 7:00 A.M. (nighttime). Unlike CNEL,  $L_{dn}$  does not include the 5 dBA adjustment (upward) to the sound levels which occur between the hours of 7:00 P.M. and 10:00 P.M. (evening).  $L_{dn}$  is typically within one dBA of CNEL and the two measurements are often used interchangeably for the purposes of defining the community noise environment and measuring A-weighted sound levels for a 24-hour period.

## **2.2 Regulatory Framework**

Government agencies have established noise standards and guidelines to protect citizens from potential hearing damage and other adverse physiological and social effects associated with

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<sup>5</sup> *State of California, General Plan Guidelines, 2003. City of West Hollywood, West Hollywood General Plan 2035, Chapter 10 Safety and Noise, September 6, 2011.*

noise. The City of West Hollywood General Plan establishes  $L_{dn}$ /CNEL guidelines for land use compatibility and includes a number of goals, objectives, and policies for land use planning purposes. The City also has regulations to control unnecessary, excessive and annoying noise, as set forth in the City of West Hollywood Noise Control Ordinance, Municipal Code Chapter 9.08. Standards and guidelines that may be applicable to this project are discussed below.

### ***2.2.1 City of West Hollywood General Plan***

The overall purpose of the General Plan is to guide policy makers in making land use determinations and in preparing noise ordinances that would limit exposure of citizens to excessive noise levels. The following City of West Hollywood General Plan policies and objectives are applicable to the Project:<sup>6</sup>

- SN-3.2: Require the inclusion of noise-reducing design features in development projects to address the impact of noise on residential development.
- SN-3.3: Review development proposals to ensure that noise standards and compatibility criteria set forth in the General Plan are met.
- SN-3.6: Require development projects to implement mitigation measures, where necessary, to reduce noise levels to meet the adopted standards and criteria. Such measures may include, but are not limited to, berms, walls, and sound attenuating architectural design and construction methods.
- SN-3.7: Require new development to meet adopted noise standards and regulations.
- SN-5.1: Work to minimize stationary noise impacts on sensitive receptors and noise emanating from construction activities, private developments/residences, landscaping activities, night clubs and bars, and special events.
- SN-5.3: Require that entertainment uses, restaurants, and bars engage in responsible management and operation to control the activities of their patrons on-site and within reasonable and legally justifiable proximity to minimize noise impacts on adjacent residences.
- SN-5.4: Require mitigation as needed for development of new nightclubs, bars, and other high noise-generating uses adjacent to residences, schools, senior citizen housing, and other noise-sensitive uses.

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<sup>6</sup> *City of West Hollywood, West Hollywood General Plan 2035, Chapter 10 Safety and Noise, September 6, 2011.*

The General Plan provides non-transportation source noise level guidance for use in determining general compatibility of proposed residential properties with adjacent properties. The noise levels represent the maximum acceptable noise levels for new developments as measured from any adjoining or proposed residential property within the City. The General Plan provides that proposed development should generally not cause, or if residential in nature, be exposed to a noise level that exceeds 55 dBA ( $L_{eq}$ ) during the daytime (8 a.m. to 10 p.m.) or 50 dBA ( $L_{eq}$ ) during the nighttime (10 p.m. to 8 a.m.).<sup>7</sup> The City's noise compatibility guidelines are provided in Table 2 (on page 12).

### 2.2.2 *City of West Hollywood Noise Control Ordinance*

Chapter 9.08, *Noise*, of the City's Municipal Code (Noise Ordinance) establishes acceptable ambient sound levels to regulate intrusive noises within specific land use zones and provides procedures and criteria for the measurement of the sound level of noise sources. These procedures recognize and account for differences in the perceived level of different types of noise and/or noise sources. The following sections of the Noise Ordinance are applicable to the proposed Project:

#### **Section 9.08.050 – Prohibited Noises – Specific Examples**

Notwithstanding any other provisions of this chapter, the following acts and the causing or permitting thereof, are declared to be in violation of this chapter.

Part a. *Radios, Phonographs, Etc.* The using, operating or permitting to be played, used or operated between the hours of 10:00 p.m. and 8:00 a.m. of any radio, musical instrument, phonograph, television set, or instrument or device similar to those heretofore specifically mentioned for the production or reproduction of sound in volume sufficiently loud as to be plainly audible at a distance of fifty feet or more therefrom.

Part k. *Commercial Establishments Adjacent to Residential Property.* Notwithstanding any provision of this code to the contrary, continuous, repeated or sustained noise from the premises of any commercial establishment which is adjacent to one or more residential dwelling units, including any outdoor area part of or under the control of the establishment, between the hours of 10:00 p.m. and 8:00 a.m. that is plainly audible from the residential dwelling unit's property line.

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<sup>7</sup> *City of West Hollywood, West Hollywood General Plan 2035, Chapter 10 Safety and Noise, September 6, 2011, Table 10-1.*

**Table 2. City of West Hollywood Guidelines for Noise Compatible Land Use**

Land Use Category	Community Noise Exposure <i>L<sub>dn</sub></i> or CNE <sub>L</sub> , dBA					
	55	60	65	70	75	80
Residential						
Transient Lodging — Motel, Hotel						
Schools, Libraries, Churches, Hospitals, Nursing Homes						
Auditoriums, Concert Halls, Amphitheaters						
Sports Arena, Outdoor Spectator Sports						
Playgrounds, Parks						
Golf Courses, Riding Stables, Water Recreation, Cemeteries						
Office Buildings, Business Commercial, and Professional						
Industrial, Manufacturing, Utilities, Agriculture						
	ZONE A – Normally Acceptable: Specified land use is satisfactory, based upon the assumption that any buildings involved meet conventional Title 24 construction standards, No special noise insulation requirements.					
	ZONE B – Conditionally Acceptable: New construction or development should be undertaken only after a detailed noise analysis is made and noise reduction measures are identified and included in the project design.					
	ZONE C – Normally Unacceptable: New construction or development is discouraged. If new construction is proposed, a detailed analysis is required, noise reduction measures must be identified, and noise insulation features included in the design.					
	ZONE D – Clearly Unacceptable: New construction or development should not be undertaken.					
Source: Table 10-2: Noise/Land Use Compatibility Matrix, West Hollywood General Plan 2035, City of West Hollywood, 2011						

**2.3 Existing Ambient Noise Levels**

Some land uses are considered more sensitive to intrusive noise than others based on the types of activities typically involved at the receptor location. Based on a review of the land uses in the Project area, a total of five noise sensitive receptor locations were selected to represent

noise sensitive uses surrounding the Project area. The locations of the five noise-sensitive receptors are identified as R1 through R5 in Figure 2 (on page 14). The nearest residential use (R4) is approximately 330 feet from the Project Site.

Ambient noise measurements were taken at the five off-site locations in the vicinity of the Project Site and one on-site location. Descriptions of the noise measurement locations are provided in Table 3 (on page 15). The off-site noise measurements locations range from approximately 60 feet (R1) to 710 feet (R2) from the Project Site. The ambient noise monitoring program was conducted using several Quest Technologies Model 2900 Integrating/Logging Sound Level Meters, these sound level meters meet and exceed the minimum industry standard performance requirements for “Type 2” standard instruments as defined in the American National Standard Institute (ANSI) S1.4.

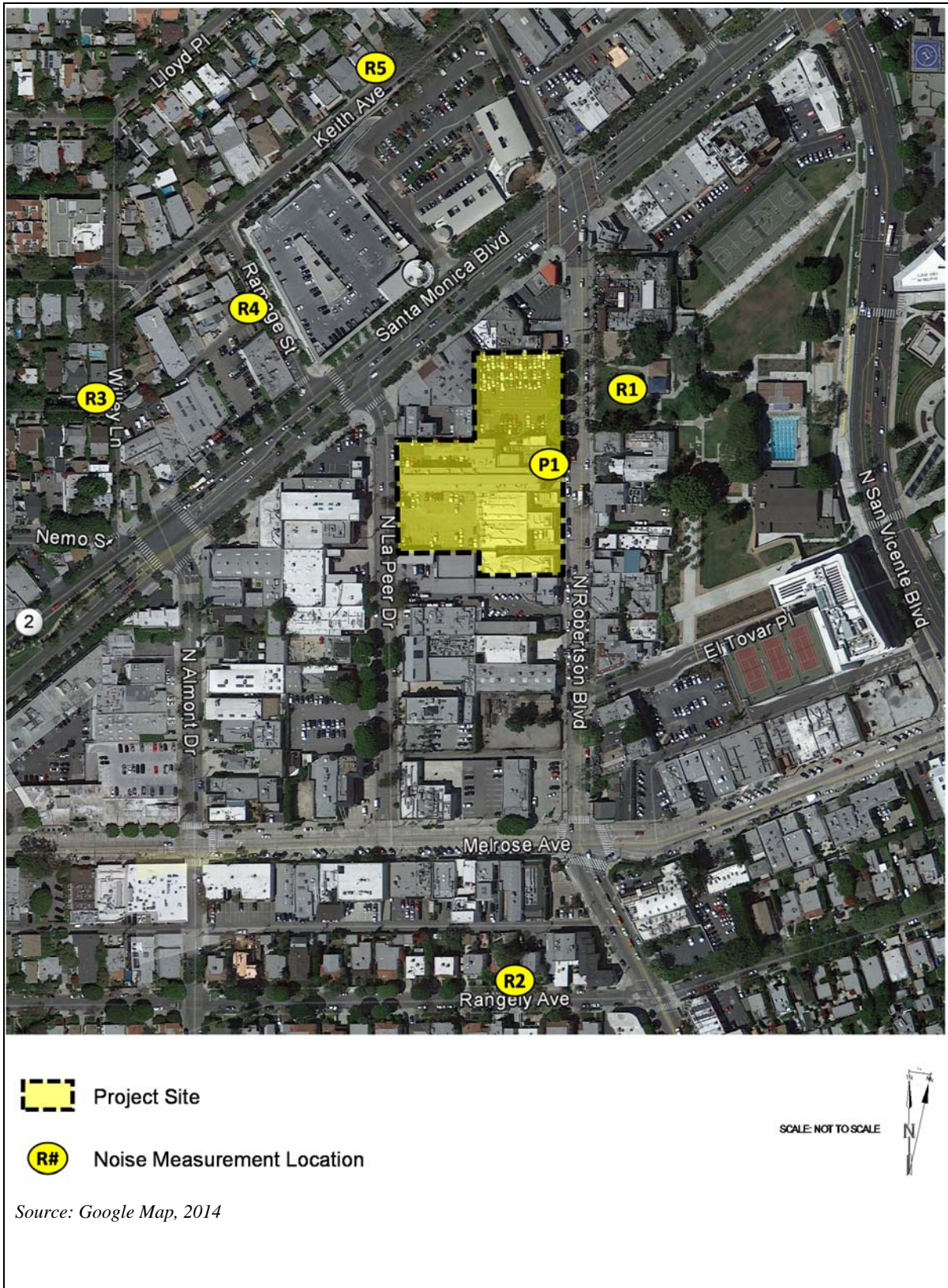
The ambient noise levels were measured between May 5 and May 6, 2014. Two 15-minute measurements were conducted at each of the off-site receptor locations during both daytime and nighttime hours. A 24-hour measurement was conducted at the Project Site (receptor P1). A 15-minute measurement is a reasonable duration for sampling ambient noise levels where street traffic is the dominant source (typical of urban environments), as traffic noise generally does not vary significantly within an hour.<sup>8</sup>

Table 4 (on page 15) presents the measured ambient noise levels at the selected receptors in  $L_{eq}$  and  $L_{90}$  in the vicinity of the Project Site. Based on field observation and measured sound data, the current ambient noise environment in the vicinity of the Project Site is controlled primarily by vehicular traffic on local roadways, and commercial uses, and other typical urban noise.

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<sup>8</sup> Caltrans, *Technical Noise Supplement, Chapter 3.3, November 2009*





**Figure 2. Noise Measurement Locations**

**Table 3. Description of Noise Measurement Locations**

Location	Description	Approximate Distance to Project Site, <sup>a</sup> Feet	Representing Nearby Land Uses	Sensitive Receptor
R1	West Hollywood Park, directly east of the Project Site	60	Public Park	Yes
R2	Residence on Rangely Avenue, south of the Project Site	710	Residential	Yes
R3	Residence at the corner of Willey Lane and Harland Avenue, west of the Project Site	510	Residential	Yes
R4	Residence on Ramage Street, north of Santa Monica Boulevard, northwest of the Project Site	330	Residential	Yes
R5	Residence on Keith Avenue, north of the Project Site	500	Residential	Yes
P1	On Project Site – Project east boundary	--	--	--

<sup>a</sup> Distances are estimated based on Google Earth map and are referenced to the Project nearest boundary.

**Table 4. Existing Ambient Noise Levels**

Location	Noise-Sensitive Land Use	Measured Ambient Noise Levels, dBA L <sub>eq</sub> /L <sub>90</sub>		CNEL (24-hour)
		Daytime Hours (8 a.m. to 10 p.m.)	Nighttime Hours (10 p.m. to 8 a.m.)	
R1	Park	58.3 / 52.6	58.8 / 55.6	63.4 <sup>a</sup>
R2	Residential	53.6 / 47.9	52.5 / 41.8	57.4 <sup>a</sup>
R3	Residential	54.4 / 47.8	49.6 / 46.1	55.7 <sup>a</sup>
R4	Residential	61.1 / 53.2	58.6 / 51.7	63.9 <sup>a</sup>
R5	Residential	62.3 / 51.3	55.1 / 48.8	62.4 <sup>a</sup>
P1	Project Site	63.8 – 68.9 / 51.8 – 65.4 <sup>b</sup>	55.8 – 66.6 / 46.6 – 55.1 <sup>b</sup>	70.2

<sup>a</sup> Estimated based on short-term (15-minute) noise measurement based on FTA procedures.  
<sup>b</sup> Measurements at Location P1 are 24-hour; therefore, a range of noise levels during the daytime and nighttime hours are provided.. The CNEL at Location P1 is calculated based on the 24-hour measurements.

### 3 IMPACT ANALYSIS

#### 3.1 Thresholds of Significance

Appendix G of the CEQA Guidelines provides a set of sample questions that address impacts with regard to noise. These questions are as follows:

Would the project result in:

- Exposure of persons to or generation of noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies;
- Exposure of persons to or generation of excessive ground-borne vibration or ground-borne noise levels;
- A substantial permanent increase in ambient noise levels in the project vicinity above levels existing without the project;
- A substantial temporary or periodic increase in ambient noise levels in the project vicinity above levels existing without the project;
- For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, exposure of people residing or working in the project area to excessive noise levels; or
- For a project within the vicinity of private airstrip, would the project expose people residing or working the project area to excessive noise levels.

With regards to these questions from Appendix G of the CEQA Guidelines, the Project Site is not located within an airport land use plan or within two miles of a public or private airport or within the vicinity of a private airstrip. Therefore, the Project would not expose people residing or working in the Project area to excessive noise levels associated with a public or private airport or from a private airstrip. As such, no further analysis of airport operation-related noise is necessary.

In addition, pursuant to Mitigation Measure 3.9-1 of the 2035 General Plan Final EIR, the City of West Hollywood has determined that the City should use the following thresholds and procedures for CEQA analysis of proposed projects:

- The City shall apply the noise standards specified in Table 10-1 and Table 10-2 of the Safety and Noise Element to proposed projects analyzed under CEQA.
- In addition, an increase in ambient noise levels is assumed to be a significant noise concern if a proposed project causes ambient noise levels to exceed the following:

- Where the existing ambient noise level is less than 60 dB, a project-related permanent increase in ambient noise levels of 5 dB  $L_{dn}$  or greater.
- Where the existing ambient noise level is greater than 60 dB, a project-related permanent increase in ambient noise levels of 3 dB  $L_{dn}$  or greater.
- A project-related temporary increase in ambient noise levels of 10 dB  $L_{eq}$  or greater.

The City of West Hollywood General Plan Final EIR does not have quantitative noise limits as applied to people gathering or outdoor amplified sound systems. However, as noted above the West Hollywood Noise Ordinance Section 9.08.050 prohibits the following:

Part a. *Radios, Phonographs, Etc.* The using, operating or permitting to be played, used or operated between the hours of 10:00 p.m. and 8:00 a.m. of any radio, musical instrument, phonograph, television set, or instrument or device similar to those heretofore specifically mentioned for the production or reproduction of sound in volume sufficiently loud as to be plainly audible at a distance of fifty feet or more therefrom.

Part k. *Commercial Establishments Adjacent to Residential Property.* Notwithstanding any provision of this code to the contrary, continuous, repeated or sustained noise from the premises of any commercial establishment which is adjacent to one or more residential dwelling units, including any outdoor area part of or under the control of the establishment, between the hours of 10:00 p.m. and 8:00 a.m. that is plainly audible from the residential dwelling unit's property line.

To ensure compliance with the West Hollywood Noise Ordinance Section 9.08.050 restrictions on noise that is "plainly audible" between the hours of 10:00 p.m. and 8:00 a.m., it has been determined that the significance threshold for the people gathering in the Project's outdoor areas or from the Project's outdoor amplified sound system between 10:00 p.m. and 8:00 a.m. (nighttime hours) would be 5 dBA below the lowest measured background sound level ( $L_{90}$ ) at the property line of the affected noise sensitive receptor during the nighttime hours. The  $L_{90}$  noise level is generally considered to represent the true background or ambient level, as it excludes intermittent peak noise sources such as a truck passing by or dog barking.

The significance threshold of 5 dBA below the lowest background sound levels measured in  $L_{90}$  is also a more conservative threshold than the City's General Plan. The General Plan provides that proposed development should generally not cause a noise level that exceeds 50 dBA ( $L_{eq}$ ) during the nighttime (10 p.m. to 8 a.m.).<sup>9</sup> As showing in Table 7, the applicable

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<sup>9</sup> *City of West Hollywood, West Hollywood General Plan 2035, Chapter 10 Safety and Noise, September 6, 2011, Table 10-1.*

nighttime thresholds for all residential sensitive receptors is below 50 dBA ( $L_{eq}$ ). Therefore, the significance threshold of 5 dBA below the lowest background sound levels measured in  $L_{90}$  is a more conservative threshold than provided in the City's General Plan, and addresses the requirement in Noise Ordinance Section 9.08.050 that new noise sources not be "plainly audible" at sensitive receptors.

Therefore, the Project would have a significant impact on noise levels from people gathering or from outdoor amplified sound systems if:

- The noise level generated at the outdoor uses, including people gathering and amplified sound systems increase the existing ambient noise level ( $L_{eq}$ ) at noise sensitive uses by 5 dBA (where the existing ambient noise level is less than 60 dBA  $L_{eq}$ ) or 3 dBA (where the existing ambient noise level is 60 dBA  $L_{eq}$  or greater), during the daytime hours between 8:00 a.m. and 10:00 p.m.; or
- The noise level generated from the outdoor uses, including people gathering and amplified sound systems, at the property line of a noise sensitive use exceeds the lowest background noise level ( $L_{90}$ ) minus 5 dBA, during the nighttime hours between 10:00 p.m. and 8:00 a.m.

### 3.2 Operation Impacts

The Project operation includes outdoor dining and outdoor meeting uses at various levels including, Level 1, Level 3, Level 4 and Level 9 of the new hotel buildings. Noise sources associated with the outdoor uses typically include noise from people gathering and conversing, and use of amplified sound systems. Table 5 (on page 19) presents the anticipated number of people at each of the outdoor spaces and the Project's proposed amplified sound levels, used for the noise analysis. The outdoor spaces at the upper levels (i.e., Levels 3, 4 and 9) would be shielded to the off-site receptors by the Project's proposed 6-ft (at Level 4) and 8-ft high (at Levels 3 and 9) solid parapet walls (translucent glass). The Project's proposed amplified sound levels and the glass parapet walls will be implemented as Project Design Features as further discussed in Section 4 (on page 21). Implementation of all Project Design Features outlined in Section 4 (on page 21) was assumed for the noise analysis.

Noise levels associated with the people gathering at the outdoor areas were assumed to be 62 dBA and 65 dBA at a distance of 3.3 feet (1 meter), for women and men speaking in raised voice effort, respectively. To represent a typical scenario, the noise analysis assumed that up to 50 percent of the people (half of which would be female and the other half male) would be talking at the same time. In addition, to represent a conservative noise scenario, the noise levels from the use of the Project's outdoor spaces were calculated based on the assumption of concurrent use of all the outdoor spaces with the maximum number of people as well as simultaneous use of the amplified sound systems. This represents a conservative worst case analysis because the Project would not be expected to operate all the outdoor spaces at capacity, concurrently.

**Table 5. Outdoor Use Assumptions**

Hotel Level	Description	Estimated Total Number of People <sup>a</sup>	Amplified Sound System Levels, dBA (L <sub>eq</sub> ) for Background Music, Banquet and Party	
			Daytime Hours (8 a.m. to 10 p.m.)	Nighttime Hours (10 p.m. to 8 a.m.)
Level 1	Outdoor dining at the northeast corner, facing Robertson Blvd.	25	75	60
	Outdoor dining at the east side, facing Robertson Blvd.	30	75	60
	Outdoor dining at the center of the Hotel (near the Lobby)	32	75	60
	Outdoor dining at the southwest corner, facing La Peer Dr.	32	75	60
Level 3	Outdoor dining at the west side, facing La Peer Dr.	64	75	55
Level 4	Outdoor meeting at the northeast corner, facing Robertson Blvd.	500	75	65
	Outdoor pool deck at the east side, facing Robertson Blvd.	316	75	65
Level 9	Outdoor dining at the northeast corner, facing Robertson Blvd.	450	85	65
	Outdoor dining at the west side, facing La Peer Dr.	270	85	65
	Outdoor dining at the southwest corner, facing La Peer Dr.	209	85	65

<sup>a</sup> Source: Hodgetts + Fung, 2016 & 2013 CA Building Code, Table 1004.1.2

Table 6 (below) presents the estimated noise levels at the off-site noise sensitive receptors from people gathering and amplified sound system at the Project’s outdoor use areas during the daytime. As indicated in Table 6, the estimated noise levels at all off-site noise-sensitive receptors would be below the daytime significance threshold.

**Table 6. Outdoor Uses Noise Levels – Daytime Hours (8 a.m. to 10 p.m.)**

Location	Estimated Noise Levels from Outdoor Areas, dBA (L <sub>eq</sub> )			Existing Daytime Ambient, dBA (L <sub>eq</sub> )	Significance Threshold, <sup>a</sup> dBA (L <sub>eq</sub> )	Significant Impact?
	People	Amplified Sound	People + Amplified Sound			
R1	48.3	62.0	62.2	58.3	63.3	No
R2	30.2	47.7	47.8	53.6	58.6	No
R3	36.3	55.9	55.9	54.4	59.4	No
R4	37.7	56.5	56.6	61.1	64.1	No
R5	37.3	54.3	54.4	62.3	65.3	No

<sup>a</sup> Significance threshold is equal to ambient plus 5 dBA where the existing ambient is less than 60 dBA and plus 3 dBA where the existing ambient is equal to or greater than 60 dBA.

Table 7 (below) presents the estimated noise levels at the off-site noise sensitive receptors from people gathering and the amplified sound at the Project’s outdoor use areas during the nighttime. As indicated in Table 7, the estimated noise levels at all off-site noise-sensitive receptors would be below the nighttime significance threshold.

**Table 7. Outdoor Uses Noise Levels – Nighttime Hours (10 p.m. to 8 a.m.)**

Location	Estimated Noise Levels from Outdoor Areas, dBA (L <sub>eq</sub> )			Nighttime Ambient Noise Levels, dBA (L <sub>90</sub> )	Nighttime Significance Threshold, <sup>a</sup> dBA (L <sub>90</sub> )	Significant Impact?
	People	Amplified Sound	People + Amplified Sound			
R1	48.3	46.2	50.4	55.6	50.6	No
R2	30.2	29.1	32.7	41.8	36.8	No
R3	36.3	36.1	39.2	46.1	41.1	No
R4	37.7	36.9	40.3	51.7	46.7	No
R5	37.3	34.7	39.2	48.8	43.8	No

<sup>a</sup> Nighttime hours significance threshold is equal to nighttime ambient L<sub>90</sub> minus 5 dBA.

## 4 PROJECT DESIGN FEATURES

As analyzed above, the outdoor uses including people gathering in the Project's outdoor areas and the use of an amplified sound system would be below the applicable significance threshold at all of the off-site noise sensitive receptors during both the daytime and nighttime hours. The following Project Design Features would be implemented as part of the Project to ensure the noise impacts would be less than significant:

- 1) The amplified sound system shall be calibrated for the outdoor uses so as to not exceed the following levels. The amplified sound system sound output is to be measured at the distance provided below on a plane parallel from the face of the speaker:
  - a. Level 1:
    - i. 75 dBA ( $L_{eq}$ ) at 15 feet, during daytime hours from 8:00 a.m. to 10:00 p.m.
    - ii. 60 dBA ( $L_{eq}$ ) at 15 feet, during nighttime hours from 10:00 p.m. to 8:00 a.m.
  - b. Level 3:
    - i. 75 dBA ( $L_{eq}$ ) at 25 feet, during daytime hours from 8:00 a.m. to 10:00 p.m.
    - ii. 55 dBA ( $L_{eq}$ ) at 25 feet, during nighttime hours from 10:00 p.m. to 8:00 a.m.
  - c. Level 4:
    - i. 75 dBA ( $L_{eq}$ ) at 35 feet, during daytime hours from 8:00 a.m. to 10:00 p.m.
    - ii. 65 dBA ( $L_{eq}$ ) at 35 feet, during nighttime hours from 10:00 p.m. to 8:00 a.m.
  - d. Level 9:
    - i. 85 dBA ( $L_{eq}$ ) at 35 feet, during daytime hours from 8:00 a.m. to 10:00 p.m.
    - ii. 65 dBA ( $L_{eq}$ ) at 35 feet, during nighttime hours from 10:00 p.m. to 8:00 a.m.
- 2) Orientate the Level 9 outdoor speaker system, such that, the sound projection from the speakers would aim toward the audience/guest area and away from the off-site noise sensitive receptors.
- 3) Provide a 6-ft high solid parapet wall (e.g., translucent glass) at the outdoor use areas at Level 4.
- 4) Provide an 8-ft high solid parapet wall (e.g., translucent glass) at the outdoor use areas at Levels 3 and 9.

With the implementation of the Project Design Features above, the estimated noise levels from use of the Project's outdoor areas (people gathering plus amplified sound) would be below the applicable significance thresholds and potential noise impacts from the Project would be less than significant.



# **Robertson Lane Hotel Project**

## **Appendices**

Provided by Acoustical Engineering Services

May 2016

Appendix A - Ambient Noise Data  
Appendix B - Noise Calculations

# Appendix A

Ambient Noise Data

Location: R1 - Park  
 Date: 5/5/2014

Time	Overload	Leq	Lmax	L10	L90
1:00:08 PM	No	56.3	61	59.2	53.2
1:01:08 PM	No	54.8	58.2	56.8	52.3
1:02:08 PM	No	55	59.2	57.5	52
1:03:08 PM	No	55.2	64.4	57.1	52.5
1:04:08 PM	No	56.4	60.2	57.7	54.6
1:05:08 PM	No	56.4	65.7	58.3	53.3
1:06:08 PM	No	60	67.3	63	52.3
1:07:08 PM	No	58.6	67.4	61	54.8
1:08:08 PM	No	56.5	62.5	58.3	53.4
1:09:08 PM	No	55.5	59.8	58.4	51.7
1:10:08 PM	No	55.3	57.7	57.1	52.8
1:11:08 PM	No	65.2	71.2	69.5	55.7
1:12:08 PM	No	59.8	67.9	63.6	53.3
1:13:08 PM	No	53.1	57.5	54.7	50.8
1:14:08 PM	No	56.9	62.7	59.5	53.7

**58.3**

Time	Overload	Leq	Lmax	L10	L90
11:53:27 PM	No	59.3	63.2	62.3	53.6
11:54:27 PM	No	56.6	58.6	57.6	55.6
11:55:27 PM	No	56.7	59.4	57.5	55.8
11:56:27 PM	No	57.2	60.9	58.2	56.2
11:57:27 PM	No	56.8	60.6	57.9	55.6
11:58:27 PM	No	58.8	61.4	60.1	57.2
11:59:27 PM	No	57.5	59.9	58.6	56.1
12:00:27 AM	No	57.2	60.3	58.9	55
12:01:27 AM	No	61.7	69.1	64.6	57.6
12:02:27 AM	No	60.4	64.7	62.8	56.2
12:03:27 AM	No	60.6	63.9	62.5	57.8
12:04:27 AM	No	58.8	62.6	61.1	52.7
12:05:27 AM	No	58.8	62.1	61.3	55.5
12:06:27 AM	No	58.5	61.7	60.7	53.1
12:07:27 AM	No	59.1	61.9	61	55.2

**58.8**

Location: R2 - Residential use on Rangely Avenue  
 Date: 5/5/2014

Time	Overload	Leq	Lmax	L10	L90
2:31:41 PM	No	51	59.1	53.5	48
2:32:41 PM	No	53.4	61.1	57.2	48.9
2:33:41 PM	No	51.8	55.4	54.2	48.1
2:34:41 PM	No	56.2	62	59.1	52.2
2:35:41 PM	No	49.2	54.2	50.7	46.9
2:36:41 PM	No	55.4	63.4	58.4	50.5
2:37:41 PM	No	52.1	60.5	54.5	48
2:38:41 PM	No	53.9	61.7	57.4	50
2:39:41 PM	No	53.8	63.3	57.7	48.6
2:40:41 PM	No	48.6	53.3	50.4	46.8
2:41:41 PM	No	52.7	63	55.3	46.9
2:42:41 PM	No	55.6	67.1	59.5	47.9
2:43:41 PM	No	51.6	61.8	52.3	47.2
2:44:41 PM	No	56.1	65.1	60.1	48.9
2:45:41 PM	No	53.5	60.1	55.5	49.2

**53.6**

Time	Overload	Leq	Lmax	L10	L90
11:23:18 PM	No	50.9	60.7	53.5	43.6
11:24:18 PM	No	49.4	57.3	52.2	45.3
11:25:18 PM	No	50.9	57.5	54.5	43.5
11:26:18 PM	No	62	79.4	58.8	44.3
11:27:18 PM	No	49.1	62.5	51.7	43.7
11:28:18 PM	No	49.5	55.8	51.9	46.3
11:29:18 PM	No	46.1	53.3	50.2	41.3
11:30:18 PM	No	46.2	55	50	41.8
11:31:18 PM	No	44.9	52.4	49.1	41.1
11:32:18 PM	No	43.5	48.8	46.4	40.7
11:33:18 PM	No	51.1	54.9	53.6	47.3
11:34:18 PM	No	47.3	53.5	50.2	43.5
11:35:18 PM	No	45.9	51.9	49.4	41.4
11:36:18 PM	No	48.9	55.9	52	44.9
11:37:18 PM	No	51.1	61	54.2	42.8

**52.5**

Location: R3 - Residential use at corner of Willey Lane and Harland Avenue  
 Date: 5/5/2014

Time	Overload	Leq	Lmax	L10	L90
1:56:01 PM	No	48.1	50.2	49.3	46.9
1:57:01 PM	No	53.5	64.4	55.5	47.2
1:58:01 PM	No	50.5	55.4	52.5	49
1:59:01 PM	No	54.2	60.8	57.7	49.7
2:00:01 PM	No	56.7	65.2	58.6	50.6
2:01:01 PM	No	53.2	58.1	56.6	49.3
2:02:01 PM	No	50.1	55.6	51.8	47.9
2:03:01 PM	No	49.3	51.1	50.2	48.4
2:04:01 PM	No	49.4	55.9	51.9	47
2:05:01 PM	No	61.5	74.8	64.6	48.6
2:06:01 PM	No	56.7	68.2	59.7	47.5
2:07:01 PM	No	53	57.8	55.5	50.4
2:08:01 PM	No	51	58.9	53.1	48.4
2:09:01 PM	No	51.8	57.2	53.4	50
2:10:01 PM	No	51.8	60.1	54.4	47.4
		<b>54.4</b>			

Time	Overload	Leq	Lmax	L10	L90
10:59:13 PM	No	48.8	52.5	50.8	45.9
11:00:13 PM	No	47.8	52.1	50.5	45.7
11:01:13 PM	No	48.5	51.7	50.6	46.1
11:02:13 PM	No	47.3	52.1	49.2	45.9
11:03:13 PM	No	48	51.9	50.5	46.3
11:04:13 PM	No	48.2	52.9	52	45.6
11:05:13 PM	No	48.3	52	50.4	46.1
11:06:13 PM	No	51.1	54.6	53.4	47
11:07:13 PM	No	47.8	49.8	48.9	46.6
11:08:13 PM	No	50.9	53.3	52.4	48.8
11:09:13 PM	No	53.1	61.3	55.8	49.3
11:10:13 PM	No	49.4	54.7	51.4	46.5
11:11:13 PM	No	48	50.3	49.3	46.7
11:12:13 PM	No	49.8	55.4	52.7	47.2
11:13:13 PM	No	51.5	54.8	53.3	49.3
		<b>49.6</b>			

Location: R4 - Residential use on Ramage Street  
 Date: 5/5/2014

Time	Overload	Leq	Lmax	L10	L90
1:37:55 PM	No	57.9	64.4	61.9	51.8
1:38:55 PM	No	56.9	64.4	58.4	54.8
1:39:55 PM	No	68.0	77.1	73.6	57.2
1:40:55 PM	No	65.6	76.8	70.2	54.8
1:41:55 PM	No	54.8	57.7	57.2	51.7
1:42:55 PM	No	57.6	62.8	59.9	54.8
1:43:55 PM	No	54.0	60.2	55.4	51.9
1:44:55 PM	No	60.5	72.2	61.9	53.5
1:45:55 PM	No	55.7	59.7	58.4	51.7
1:46:55 PM	No	58.3	65.7	59.7	53.8
1:47:55 PM	No	57.2	60.9	59	54.5
1:48:55 PM	No	61.3	69	66.1	54.8
1:49:55 PM	No	58.6	68.6	61.6	54.6
1:50:55 PM	No	56.7	61.9	58.7	54.2
1:51:55 PM	No	62.5	72.5	65.7	54.6

**61.1**

Time	Overload	Leq	Lmax	Lpeak	L10	L90
10:42:19 PM	No	65.6	73.6	70.6	54.9	
10:43:19 PM	No	59.3	68.4	64	52.7	
10:44:19 PM	No	56.2	60.4	58.6	52.9	
10:45:19 PM	No	55.8	64	58.4	52.2	
10:46:19 PM	No	57.0	64.9	59.4	53.1	
10:47:19 PM	No	57.6	69.6	60.4	50.5	
10:48:19 PM	No	56.1	61.8	58.5	51.7	
10:49:19 PM	No	57.4	62.6	59.7	53.3	
10:50:19 PM	No	55.7	62.6	59.9	50.4	
10:51:19 PM	No	56.3	64.7	58.5	51.6	
10:52:19 PM	No	57.3	61	60.3	52.3	
10:53:19 PM	No	54.4	58.3	56.6	51.7	
10:54:19 PM	No	57.1	62.3	59.3	52	
10:55:19 PM	No	54.2	60.4	57	50.2	
10:56:19 PM	No	60.3	72.1	63.1	52.9	

**58.6**

Location: R5 - Residential use on Keith Avenue  
 Date: 5/5/2014

Time	Overload	Leq	Lmax	L10	L90
1:20:40 PM	No	63.6	76.6	66.4	52.3
1:21:40 PM	No	60.8	72.1	62.5	51.1
1:22:40 PM	No	66	73.8	72.2	52.8
1:23:40 PM	No	62.1	72.6	67.2	52
1:24:40 PM	No	57.4	70.1	57.1	50.9
1:25:40 PM	No	59.2	67.3	64.1	51.9
1:26:40 PM	No	54.4	58.8	57.7	51.3
1:27:40 PM	No	62.5	74.9	66.8	51.5
1:28:40 PM	No	60.1	70.2	65	49.7
1:29:40 PM	No	60.6	71.1	65.6	49.3
1:30:40 PM	No	63.5	73.7	68.9	51.9
1:31:40 PM	No	58.9	70	60.8	53
1:32:40 PM	No	67.1	80.8	68.9	51.7
1:33:40 PM	No	58.4	69.4	62.9	50.2
1:34:40 PM	No	63.3	72.6	68.2	53

**62.3**

Time	Overload	Leq	Lmax	L10	L90
10:21:12 PM	No	56.7	66.3	61.5	48.3
10:22:12 PM	No	60.8	70.9	65.5	50.9
10:23:12 PM	No	57.5	64	60.7	49.2
10:24:12 PM	No	52.3	63.4	53.3	49.3
10:25:12 PM	No	57.8	71.1	59.3	50
10:26:12 PM	No	50.8	54.6	51.6	49.6
10:27:12 PM	No	50.5	53.5	51.5	49.4
10:28:12 PM	No	49.8	53.2	51.8	48.5
10:29:12 PM	No	49.3	53.9	50.4	48.3
10:30:12 PM	No	49.7	51.8	50.3	48.9
10:31:12 PM	No	51.6	58.4	53.9	48.6
10:32:12 PM	No	53.3	62.4	56.5	49.1
10:33:12 PM	No	56	67.8	58	48.8
10:34:12 PM	No	50.4	55.3	53	48.5
10:35:12 PM	No	56.1	67.6	58.7	50.3

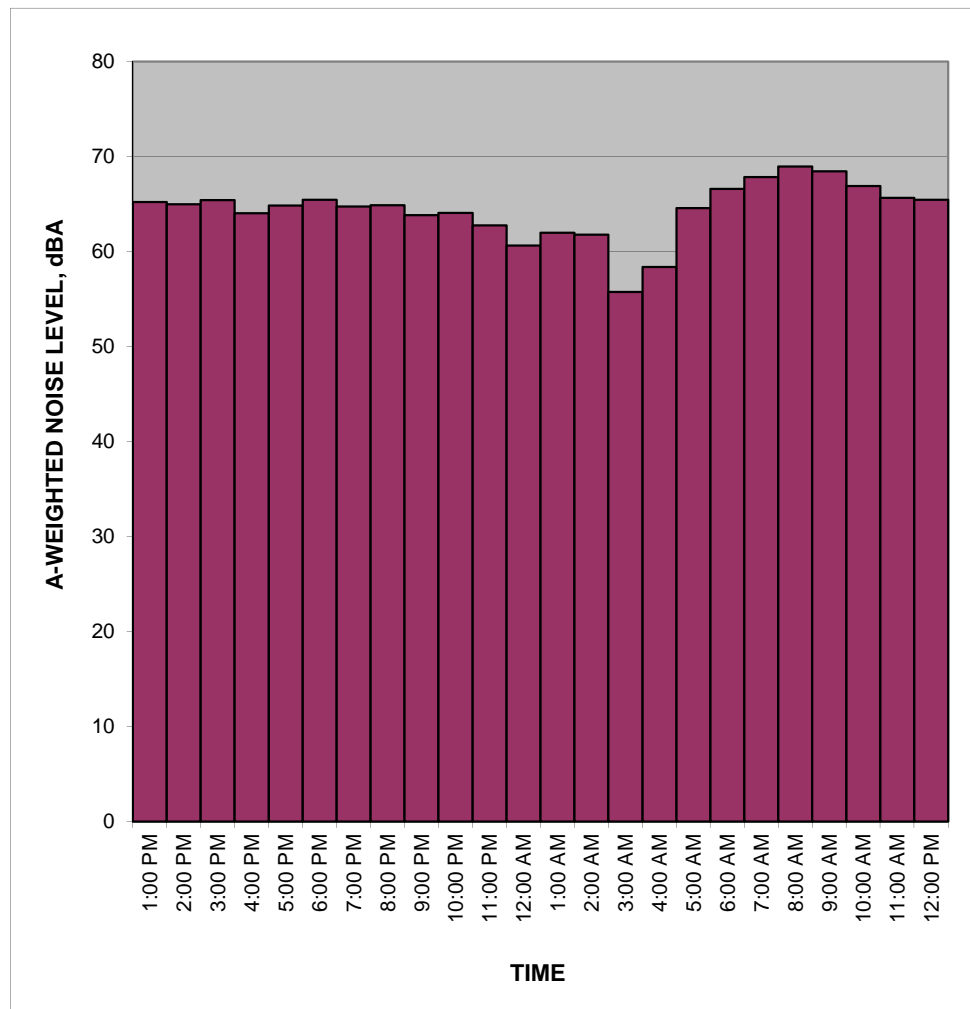
**55.1**

# Measured Ambient Noise Levels

Project: Robertson Lane Hotel  
 Location: P1 - Project Site  
 Sources: Traffic Volumes

Date: 5/5 to 5/6/2014

<i>TIME</i>	<i>HNL, dB(A)</i>
1:00 PM	65.2
2:00 PM	65.0
3:00 PM	65.4
4:00 PM	64.0
5:00 PM	64.8
6:00 PM	65.5
7:00 PM	64.7
8:00 PM	64.9
9:00 PM	63.8
10:00 PM	64.1
11:00 PM	62.8
12:00 AM	60.6
1:00 AM	62.0
2:00 AM	61.8
3:00 AM	55.8
4:00 AM	58.4
5:00 AM	64.6
6:00 AM	66.6
7:00 AM	67.8
8:00 AM	68.9
9:00 AM	68.4
10:00 AM	66.9
11:00 AM	65.6
12:00 PM	65.4
<b>CNEL, dB(A):</b>	<b>70.2</b>



**NOTES:**



# Appendix B

Noise Calculations

## Robertson Lane Hotel

### Octave spectra of the sources in dB(A) - Level 9 - Speakers

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level9_Speakers-B	117.	SoundSystem	98.3	103.4	105.9	106.3	109.5	110.7	110.5	108.4
Level9_Speakers-C	117.	SoundSystem	98.3	103.4	105.9	106.3	109.5	110.7	110.5	108.4
Level9_Speakers-D	117.	SoundSystem	98.3	103.4	105.9	106.3	109.5	110.7	110.5	108.4
Level9_Speakers-A	117.	SoundSystem	98.3	103.4	105.9	106.3	109.5	110.7	110.5	108.4

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## Robertson Lane Hotel

### Octave spectra of the sources in dB(A) - Level 9 - People

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level9_People-A(450/2)	95.3	People (Raised Voice)	48.5	58.5	75.0	90.4	91.6	87.8	82.6	72.5
Level9_People-B(450/2)	95.3	People (Raised Voice)	48.5	58.5	75.0	90.4	91.6	87.8	82.6	72.5
Level9_People-C(270)	96.1	People (Raised Voice)	49.3	59.3	75.8	91.2	92.4	88.6	83.4	73.3
Level9_People-D(209)	95.0	People (Raised Voice)	48.2	58.2	74.7	90.1	91.3	87.5	82.3	72.2

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## Robertson Lane Hotel

### Octave spectra of the sources in dB(A) - Level 4 - Speakers

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level4-Speakers-A	107.	SoundSystem(1)	73.8	83.9	91.4	96.8	100.0	101.2	101.0	98.9
Level4-Speakers-B	107.	SoundSystem(1)	73.8	83.9	91.4	96.8	100.0	101.2	101.0	98.9

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## Robertson Lane Hotel

### Octave spectra of the sources in dB(A) - Level 4 - People

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level4-People-A(500)	98.8	People (Raised Voice)	52.0	62.0	78.5	93.9	95.1	91.3	86.1	76.0
Level4-People-B(316)	96.8	People (Raised Voice)	50.0	60.0	76.5	91.9	93.1	89.3	84.1	74.0

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## Robertson Lane Hotel

### Octave spectra of the sources in dB(A) - Level 3 - Speakers

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level3-Speakers	104.	SoundSystem	85.3	90.4	92.9	93.3	96.5	97.7	97.5	95.4

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## Robertson Lane Hotel

### Octave spectra of the sources in dB(A) - Level 3 - People

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level3-People(64)	89.8	People (Raised Voice)	43.0	53.0	69.5	84.9	86.1	82.3	77.1	67.0



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## Robertson Lane Hotel

### Octave spectra of the sources in dB(A) - Level 1- Speakers

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level1-Speakers-A	99.0	SoundSystem	80.3	85.4	87.9	88.3	91.5	92.7	92.5	90.4
Level1-Speakers-B	99.0	SoundSystem	80.3	85.4	87.9	88.3	91.5	92.7	92.5	90.4
Level1-Speakers-C	99.0	SoundSystem	80.3	85.4	87.9	88.3	91.5	92.7	92.5	90.4
Level1-Speakers-D	99.0	SoundSystem	80.3	85.4	87.9	88.3	91.5	92.7	92.5	90.4

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**Robertson Lane Hotel**  
**Octave spectra of the sources in dB(A) - Level 1- People**

Name	Lw dB(A)	Emission spectrum	63Hz dB(A)	125Hz dB(A)	250Hz dB(A)	500Hz dB(A)	1kHz dB(A)	2kHz dB(A)	4kHz dB(A)	8kHz dB(A)
Level1-PeopleA(25)	85.9	People (Raised Voice)	39.1	49.1	65.6	81.0	82.2	78.4	73.2	63.1
Level1-PeopleB(30)	86.6	People (Raised Voice)	39.8	49.8	66.3	81.7	82.9	79.1	73.9	63.8
Level1-PeopleC(32)	86.8	People (Raised Voice)	40.0	50.0	66.5	81.9	83.1	79.3	74.1	64.0
Level1-PeopleD(32)	86.8	People (Raised Voice)	40.0	50.0	66.5	81.9	83.1	79.3	74.1	64.0

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**Robertson Lane Hotel**  
**Assessed contibution level - Level 9 - Speakers**

Source	Leq,d dB(A)	Leq,n dB(A)	
<b>Receiver R1</b>	<b>Leq,d 57.9</b>	<b>dB(A)</b>	<b>Leq,n 37.9</b> <b>dB(A)</b>
Level8_Speakers-B	55.5	35.5	
Level8_Speakers-C	42.9	22.9	
Level8_Speakers-D	52.3	32.3	
Level8_Speakers-A	48.9	28.9	
<b>Receiver R2</b>	<b>Leq,d 47.3</b>	<b>dB(A)</b>	<b>Leq,n 27.3</b> <b>dB(A)</b>
Level8_Speakers-B	41.8	21.8	
Level8_Speakers-C	40.8	20.8	
Level8_Speakers-D	43.6	23.6	
Level8_Speakers-A	36.2	16.2	
<b>Receiver R3</b>	<b>Leq,d 55.5</b>	<b>dB(A)</b>	<b>Leq,n 35.5</b> <b>dB(A)</b>
Level8_Speakers-B	41.5	21.5	
Level8_Speakers-C	51.4	31.4	
Level8_Speakers-D	49.4	29.4	
Level8_Speakers-A	50.5	30.5	
<b>Receiver R4</b>	<b>Leq,d 55.8</b>	<b>dB(A)</b>	<b>Leq,n 35.8</b> <b>dB(A)</b>
Level8_Speakers-B	42.4	22.4	
Level8_Speakers-C	52.4	32.4	
Level8_Speakers-D	50.2	30.2	
Level8_Speakers-A	49.0	29.0	
<b>Receiver R5</b>	<b>Leq,d 54.2</b>	<b>dB(A)</b>	<b>Leq,n 34.2</b> <b>dB(A)</b>
Level8_Speakers-B	43.2	23.2	
Level8_Speakers-C	48.5	28.5	
Level8_Speakers-D	42.3	22.3	
Level8_Speakers-A	51.8	31.8	

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**Robertson Lane Hotel**  
**Assessed contibution level - Level 9 - People**

**9**

Source	Leq,d dB(A)	Leq,n dB(A)	
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Receiver R1	Leq,d 36.9		dB(A)	Leq,n 36.9		dB(A)
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Level9_People-A(450/2)	30.8	30.8				
Level9_People-B(450/2)	34.0	34.0				
Level8_People-C(270)	20.8	20.8				
Level8_People-D(209)	30.4	30.4				

Receiver R2	Leq,d 25.9		dB(A)	Leq,n 25.9		dB(A)
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Level9_People-A(450/2)	18.9	18.9				
Level9_People-B(450/2)	19.8	19.8				
Level8_People-C(270)	19.4	19.4				
Level8_People-D(209)	21.3	21.3				

Receiver R3	Leq,d 34.6		dB(A)	Leq,n 34.6		dB(A)
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Level9_People-A(450/2)	28.8	28.8				
Level9_People-B(450/2)	20.2	20.2				
Level8_People-C(270)	31.4	31.4				
Level8_People-D(209)	27.9	27.9				

Receiver R4	Leq,d 34.8		dB(A)	Leq,n 34.8		dB(A)
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Level9_People-A(450/2)	25.8	25.8				
Level9_People-B(450/2)	21.1	21.1				
Level8_People-C(270)	32.7	32.7				
Level8_People-D(209)	28.4	28.4				

Receiver R5	Leq,d 32.9		dB(A)	Leq,n 32.9		dB(A)
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Level9_People-A(450/2)	28.5	28.5				
Level9_People-B(450/2)	27.1	27.1				
Level8_People-C(270)	27.9	27.9				
Level8_People-D(209)	20.0	20.0				

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**Robertson Lane Hotel**  
**Assessed contibution level - Level 4 - Speakers**

Source	Leq,d dB(A)	Leq,n dB(A)	
Receiver R1	Leq,d 48.9		dB(A) Leq,n 38.9 dB(A)
Level4-Speakers-A	45.7	35.7	
Level4-Speakers-B	46.1	36.1	
Receiver R2	Leq,d 34.0		dB(A) Leq,n 24.0 dB(A)
Level4-Speakers-A	29.8	19.8	
Level4-Speakers-B	31.9	21.9	
Receiver R3	Leq,d 31.8		dB(A) Leq,n 21.8 dB(A)
Level4-Speakers-A	27.0	17.0	
Level4-Speakers-B	30.0	20.0	
Receiver R4	Leq,d 33.0		dB(A) Leq,n 23.0 dB(A)
Level4-Speakers-A	29.1	19.1	
Level4-Speakers-B	30.7	20.7	
Receiver R5	Leq,d 35.1		dB(A) Leq,n 25.1 dB(A)
Level4-Speakers-A	33.5	23.5	
Level4-Speakers-B	30.1	20.1	

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**Robertson Lane Hotel**  
**Assessed contibution level - Level 4 - People**

Source	Leq,d dB(A)	Leq,n dB(A)	
Receiver R1	Leq,d 42.1		dB(A) Leq,n 42.1 dB(A)
Level4-People-A(500)	40.1	40.1	
Level4-People-B(316)	37.7	37.7	
Receiver R2	Leq,d 27.7		dB(A) Leq,n 27.7 dB(A)
Level4-People-A(500)	24.8	24.8	
Level4-People-B(316)	24.5	24.5	
Receiver R3	Leq,d 27.3		dB(A) Leq,n 27.3 dB(A)
Level4-People-A(500)	24.2	24.2	
Level4-People-B(316)	24.4	24.4	
Receiver R4	Leq,d 26.5		dB(A) Leq,n 26.5 dB(A)
Level4-People-A(500)	23.2	23.2	
Level4-People-B(316)	23.7	23.7	
Receiver R5	Leq,d 35.2		dB(A) Leq,n 35.2 dB(A)
Level4-People-A(500)	34.8	34.8	
Level4-People-B(316)	25.2	25.2	

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**Robertson Lane Hotel**  
**Assessed contibution level - Level 3 - People**

Source	Leq,d dB(A)	Leq,n dB(A)	
Receiver R1	Leq,d 19.6		dB(A) Leq,n 19.6 dB(A)
Level3-People(64)	19.6	19.6	
Receiver R2	Leq,d 17.9		dB(A) Leq,n 17.9 dB(A)
Level3-People(64)	17.9	17.9	
Receiver R3	Leq,d 28.2		dB(A) Leq,n 28.2 dB(A)
Level3-People(64)	28.2	28.2	
Receiver R4	Leq,d 31.1		dB(A) Leq,n 31.1 dB(A)
Level3-People(64)	31.1	31.1	
Receiver R5	Leq,d 17.9		dB(A) Leq,n 17.9 dB(A)
Level3-People(64)	17.9	17.9	

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**Robertson Lane Hotel**  
**Assessed contibution level - Level 1- Speakers**

Source	Leq,d dB(A)	Leq,n dB(A)	
<b>Receiver R1</b>	<b>Leq,d 59.5</b>	<b>dB(A)</b>	<b>Leq,n 44.5</b> <b>dB(A)</b>
Level1-Speakers-A	56.9	41.9	
Level1-Speakers-B	56.0	41.0	
Level1-Speakers-C	32.9	17.9	
Level1-Speakers-D	26.2	11.2	
<b>Receiver R2</b>	<b>Leq,d 23.2</b>	<b>dB(A)</b>	<b>Leq,n 8.2</b> <b>dB(A)</b>
Level1-Speakers-A	18.6	3.6	
Level1-Speakers-B	15.9	0.9	
Level1-Speakers-C	16.8	1.8	
Level1-Speakers-D	17.2	2.2	
<b>Receiver R3</b>	<b>Leq,d 36.0</b>	<b>dB(A)</b>	<b>Leq,n 21.0</b> <b>dB(A)</b>
Level1-Speakers-A	16.9	1.9	
Level1-Speakers-B	16.9	1.9	
Level1-Speakers-C	20.1	5.1	
Level1-Speakers-D	35.8	20.8	
<b>Receiver R4</b>	<b>Leq,d 40.8</b>	<b>dB(A)</b>	<b>Leq,n 25.8</b> <b>dB(A)</b>
Level1-Speakers-A	20.2	5.2	
Level1-Speakers-B	19.9	4.9	
Level1-Speakers-C	22.4	7.4	
Level1-Speakers-D	40.6	25.6	
<b>Receiver R5</b>	<b>Leq,d 28.0</b>	<b>dB(A)</b>	<b>Leq,n 13.0</b> <b>dB(A)</b>
Level1-Speakers-A	20.8	5.8	
Level1-Speakers-B	19.2	4.2	
Level1-Speakers-C	18.6	3.6	
Level1-Speakers-D	25.6	10.6	

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## Robertson Lane Hotel Assessed contibution level - Level 1- People

Source	Leq,d dB(A)	Leq,n dB(A)	
<b>Receiver R1</b>	<b>Leq,d 46.6</b>	<b>dB(A)</b>	<b>Leq,n 46.6</b> <b>dB(A)</b>
Level1-PeopleA(25)	43.4	43.4	
Level1-PeopleB(30)	43.8	43.8	
Level1-PeopleC(32)	14.6	14.6	
Level1-PeopleD(32)	20.1	20.1	
<b>Receiver R2</b>	<b>Leq,d 10.4</b>	<b>dB(A)</b>	<b>Leq,n 10.4</b> <b>dB(A)</b>
Level1-PeopleA(25)	3.9	3.9	
Level1-PeopleB(30)	3.6	3.6	
Level1-PeopleC(32)	5.5	5.5	
Level1-PeopleD(32)	4.3	4.3	
<b>Receiver R3</b>	<b>Leq,d 22.6</b>	<b>dB(A)</b>	<b>Leq,n 22.6</b> <b>dB(A)</b>
Level1-PeopleA(25)	4.2	4.2	
Level1-PeopleB(30)	4.9	4.9	
Level1-PeopleC(32)	22.4	22.4	
Level1-PeopleD(32)	6.8	6.8	
<b>Receiver R4</b>	<b>Leq,d 30.6</b>	<b>dB(A)</b>	<b>Leq,n 30.6</b> <b>dB(A)</b>
Level1-PeopleA(25)	7.7	7.7	
Level1-PeopleB(30)	8.1	8.1	
Level1-PeopleC(32)	30.5	30.5	
Level1-PeopleD(32)	10.2	10.2	
<b>Receiver R5</b>	<b>Leq,d 14.8</b>	<b>dB(A)</b>	<b>Leq,n 14.8</b> <b>dB(A)</b>
Level1-PeopleA(25)	6.9	6.9	
Level1-PeopleB(30)	7.1	7.1	
Level1-PeopleC(32)	11.9	11.9	
Level1-PeopleD(32)	6.4	6.4	

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