

# City of West Hollywood Community Meeting

Presented by  
Daniel Zepeda, SE  
Jeff Roi, SE

Date: November 29, 2016

## Non-Ductile Concrete



**1971 SYLMAR EARTHQUAKE**

## Non-Ductile Concrete



**1985 MEXICO CITY EARTHQUAKE**

<http://www.gettyimages.it/evento/years-since-the-mexico-city-earthquake-572224691#toppled-by-one-of-the-deadliest-earthquakes-of-the-century-mexico-picture-id107295750>

## Non-Ductile Concrete



**1989 LOMA PRIETA EARTHQUAKE**

[https://en.wikipedia.org/wiki/1989\\_Loma\\_Prieta\\_earthquake](https://en.wikipedia.org/wiki/1989_Loma_Prieta_earthquake)

## Non-Ductile Concrete



**1994 NORTHRIDGE EARTHQUAKE**

<http://sfvmedia.com/sfv/ventura-blvd-buildings-earthquake-risk/#lightbox/0/>

## Non-Ductile Concrete



**1995 KOBE EARTHQUAKE**

<http://www.ngdc.noaa.gov/hazardimages/event/show/19>

## Non-Ductile Concrete



**1999 CHI-CHI EARTHQUAKE**

<https://www.youtube.com/watch?v=8cqQJcmLWQ>

## Non-Ductile Concrete



**2003 BINGOL TURKEY EARTHQUAKE**

<http://hutpedia.blogspot.com/2011/10/earthquake-72-magnitude-hits-turkey.html>

## Non-Ductile Concrete



### **2005 PAKISTAN EARTHQUAKE**

<http://www.nydailynews.com/news/world/quake-terrorizes-pakistan-india-afghanistan-2005-article-1.2369675>

## Non-Ductile Concrete



### **2010 HAITI EARTHQUAKE**

<https://www.wired.com/2010/02/earthquake-proofing-haiti/>

## Non-Ductile Concrete



### **2011 CHRISTCHURCH NEW ZEALAND EARTHQUAKE**

<http://www.stuff.co.nz/the-press/news/christchurch-earthquake-2011/66404258/Christchurch-quake-survivors-lives-irrevocably-changed>

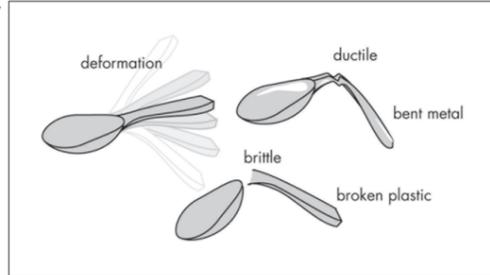
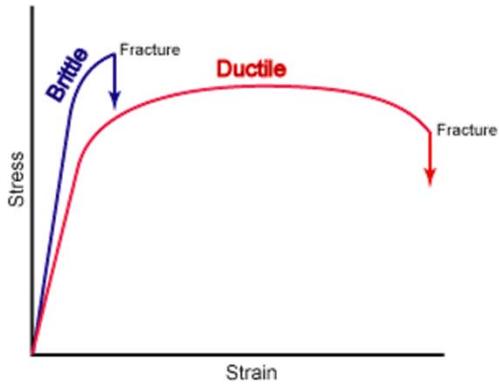
## Non-Ductile Concrete



### **2016 TAIWAN EARTHQUAKE**

<https://sputniknews.com/asia/201602101034481762-taiwan-arrests-developers-earthquake/>

# Ductility vs Strength



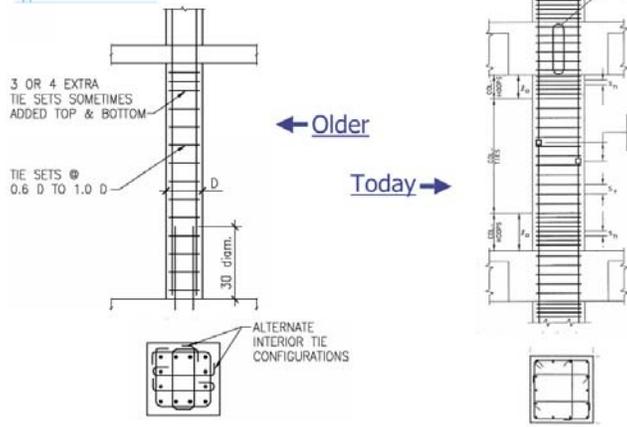
<http://ficientdesign.com/wp-content/uploads/2010/06/Brittle-Ductile-Stress-Strain.gif>  
[https://www.fema.gov/media-library-data/20130726-1556-20490-5679/fema454\\_complete.pdf](https://www.fema.gov/media-library-data/20130726-1556-20490-5679/fema454_complete.pdf)

# Non-Ductile Concrete



# Non-Ductile Concrete

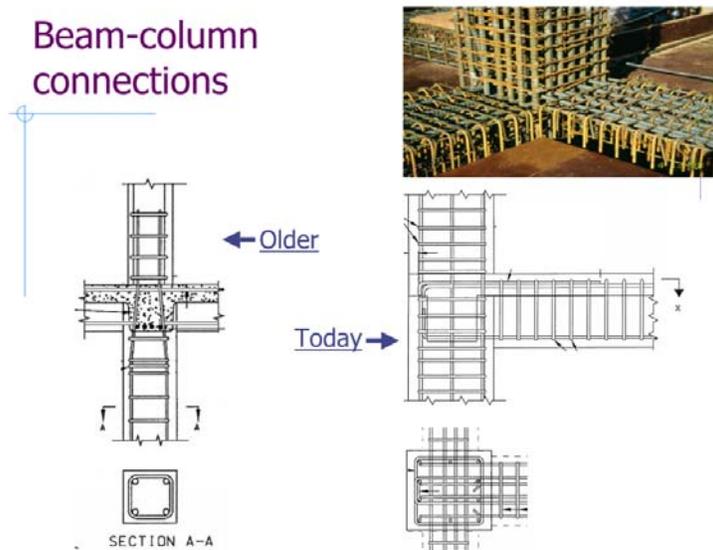
## Columns



EERI / PEER Historic Overview Presentation by Jack Moehle, UC Berkeley

# Non-Ductile Concrete

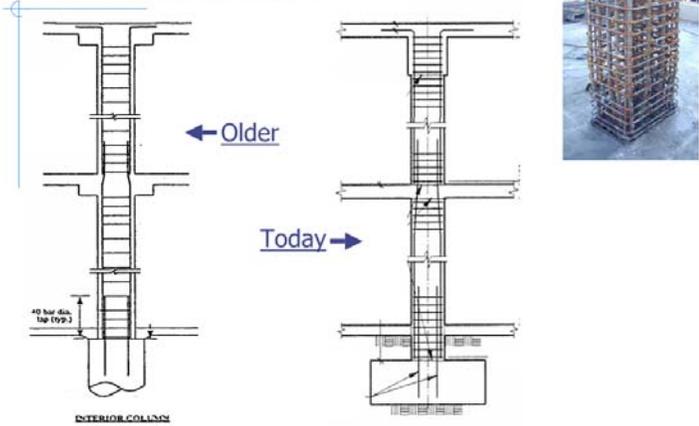
## Beam-column connections



EERI / PEER Historic Overview Presentation by Jack Moehle, UC Berkeley

# Non-Ductile Concrete

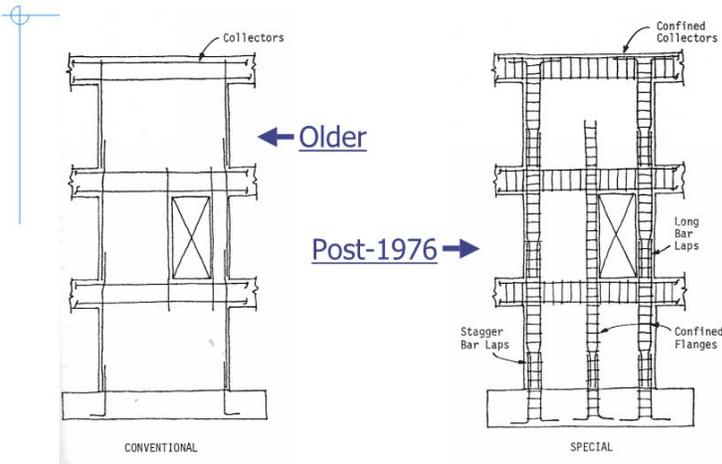
## Gravity columns



EERI / PEER Historic Overview Presentation by Jack Moehle, UC Berkeley

# Non-Ductile Concrete

## Walls



EERI / PEER Historic Overview Presentation by Jack Moehle, UC Berkeley

# Pre-Northridge Steel Moment Frames



**1994 NORTHRIDGE EARTHQUAKE**

# Pre-Northridge Steel Moment Frames

FEDERAL EMERGENCY MANAGEMENT AGENCY FEMA-355E / September, 2000

State of the Art Report on Past Performance of Steel Moment-Frame Buildings in Earthquakes

Program to Reduce the Earthquake Hazards of Steel Moment-Frame Structures

Nevertheless, the Northridge earthquake exposed a faulty detail that performed in the field much as it had in the lab for twenty years. Most of the connections survived. Too many failed. In many ways, this report merely updates a 1991 study of the past performance of steel structures in earthquakes (Yanev et al., 1991). That report captured the pre-Northridge thinking of the entire design and construction community—both the right and wrong of it—in a single short paragraph:

When failures of steel structures occur, connection failures are the most common cause. No advantage can be derived from the strength and ductility of a steel member if its connections fail prematurely. However, use of industry-standard details generally provides acceptable performance.

**1994 NORTHRIDGE EARTHQUAKE**

<http://www.nehrp.gov/pdf/fema355e.pdf>

# Pre-Northridge Steel Moment Frames

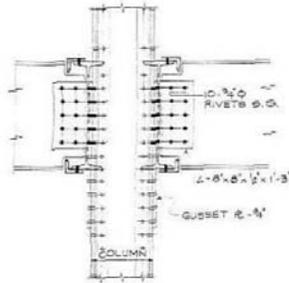


Figure 2-1 Riveted Beam-Column Connection, Pre-1920s

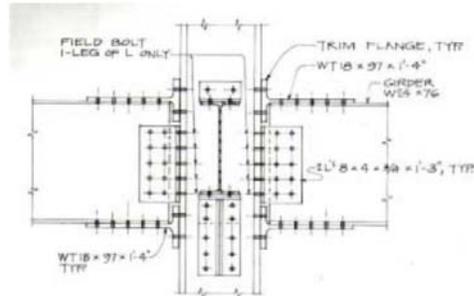


Figure 2-2 Bolted and Riveted Connection, 1930s

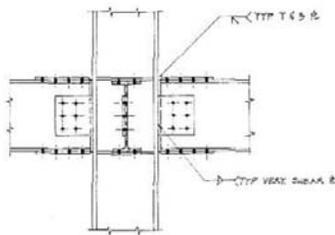


Figure 2-3 Welded and Bolted Moment Connection, 1950-1960

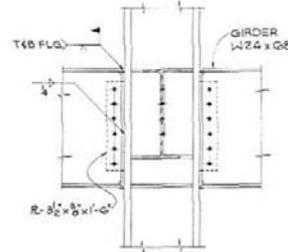


Figure 2-4 Welded Moment Connection, 1980s

## 1994 NORTHRIDGE EARTHQUAKE

<http://www.nehrp.gov/pdf/fema355e.pdf>

# Pre-Northridge Steel Moment Frames

Table 5-2 Damage by Structure Type in Selected North American Earthquakes of the WSMF Era

Earthquake	Wood frame residential	Unreinforced Masonry	Precast Concrete	Concrete frame or wall	Steel frames
Prince William Sound, 1964	Excellent performance (Wood, 1967).	Not a common construction type in the area.	Typically slight to moderate damage, less than expected (Wood, 1967).	1-5 story; generally no significant structural damage, one partial collapse. Taller: considerable structural damage.	Inconclusive. Considerable structural damage, but only a few buildings had complete steel frames.
San Fernando, 1971	Majority of buildings under 20% loss. Most structural damage in foundation anchorage and open fronts.	Moderate or severe damage to half of brick buildings in downtown San Fernando.	Multiple tilt-up collapses.	Many collapses generally caused by poor ductility and irregularities.	No significant structural damage was observed in general. Cracked welds observed in two buildings under construction.
Mexico City, 1985	Not a common building type in the area.	Many URMs severely damaged. Wall-floor connections and out-of-plane failures.	Not a common construction type in the area.	7-15 story, frame and infill structures heavily damaged or collapsed. Similar low-rise structures perform better (Bertero and Miranda, 1989).	Some pre-1950 steel frames collapsed. Collapse of isolated braced frame buildings due to column failure. Little other moment frame damage reported.
Loma Prieta, 1989	Severe damage to wood structures with open fronts or tuck-under parking, especially on soft soils.	Many URMs severely damaged or collapsed. Wall-floor connections and out-of-plane failures.	Many examples of connection damage although collapses were uncommon.	Nonductile frames and wall structures damaged, including fatal freeway collapse. Newer structures generally performed well.	Five buildings known to have slight to significant weld damage, some discovered only upon post-Northridge inspection.
Northridge, 1994	Severe damage to multi-story wood structures with tuck-under parking.	Many URMs damaged but many collapses avoided by previous retrofits.	Many examples of connection damage and several significant collapses.	Older structures, including freeways. Newer structures generally performed well. Deflection compatibility issues noted.	Widespread, unexpected connection damage, several buildings declared unsafe, at least one irreparable. No collapses.

Note: See Table 5-1 for additional information and references.

## 1994 NORTHRIDGE EARTHQUAKE

<http://www.nehrp.gov/pdf/fema355e.pdf>

inspection.  
Widespread, unexpected connection damage, several buildings declared unsafe, at least one irreparable. No collapses.

# Pre-Northridge Steel Moment Frames

ABOUT 60% OF INSPECTED BUILDINGS  
HAD SOME LEVEL OF DAMAGE

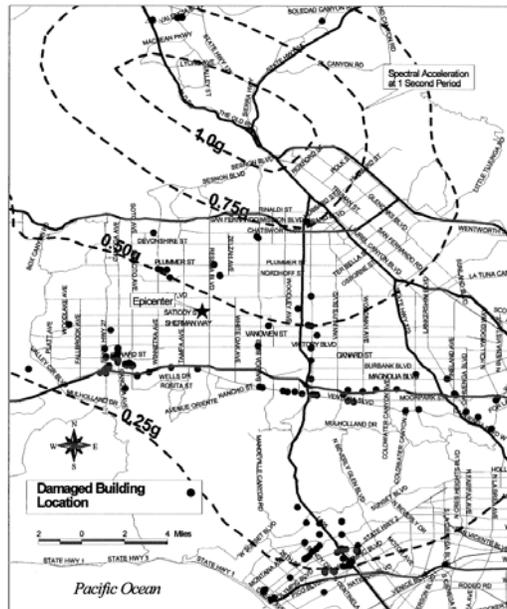
**Table 6-2 Number of WSMF Buildings with Various Northridge Earthquake Damage Rates**

	1 story	2-4 story	5-12 story	13+ story	All
All buildings	13	69	47	26	155
No damage	11	26	16	12	65
$0 < DR \leq .05$	0	7	6	5	18
$.051 < DR \leq .10$	0	10	8	1	19
$.11 < DR \leq .20$	0	12	11	6	29
$.21 < DR \leq .50$	2	13	4	2	21
$DR > .50$	0	1	2	0	3
Shear damage	0	9	10	4	23
Panel zone damage	1	16	8	4	29

## 1994 NORTHRIDGE EARTHQUAKE

<http://www.nehrp.gov/pdf/fema355e.pdf>

# Pre-Northridge Steel Moment Frames



**Figure B-4 Spatial Distribution of Damaged Buildings  
1994 NORTHRIDGE EARTHQUAKE**

<http://www.nehrp.gov/pdf/fema355e.pdf>



3/11/2011 M 9.1 Tohoku Japan (2016 M7.0)



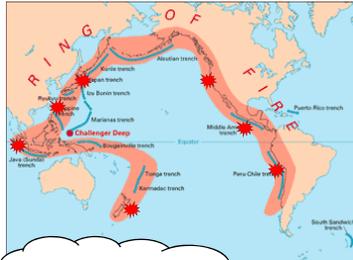
8/24/14 M 6.0 NAPA, USA



11/07/2012 M 7.4 Guatemala and Mexico



12/26/2004 M 9.1 Sumatra, Indonesia (2005 M8.6, 2007 M7.9, 2007 M8.4, 2010 M7.9)



<https://www.usgs.gov/>



2/27/2010 M 8.8 Maule, Chile (2014 M8.1)



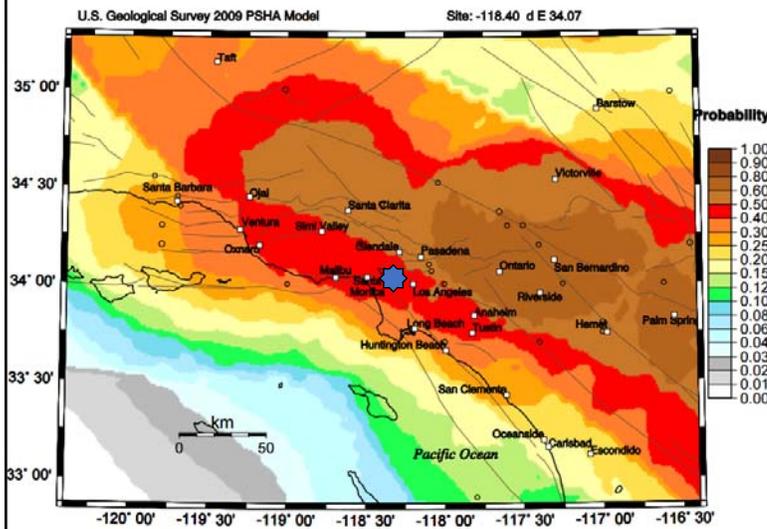
2/6/2016 M 6.4 Meining, Taiwan (2016 M)



2/22/2011 M 6.3 Christchurch, New Zealand (2013 M6.6)

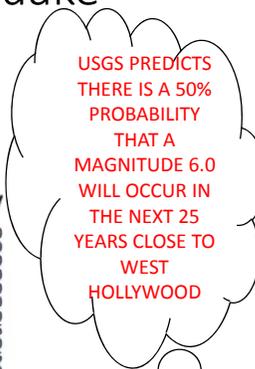
## Probability of Next Earthquake

Probability of earthquake with M > 6.0 within 25 years & 50 km

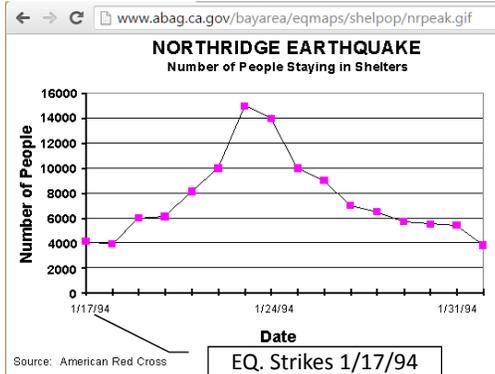


GMT 2015 Oct 22 02:17:26 80 probabilities from USGS GFR 88-1128 PSHA, 50 km maximum horizontal distance. Site of interest: Ingleton. Fault traces are brown, rivers blue. Epicenters M=6.0 circles.

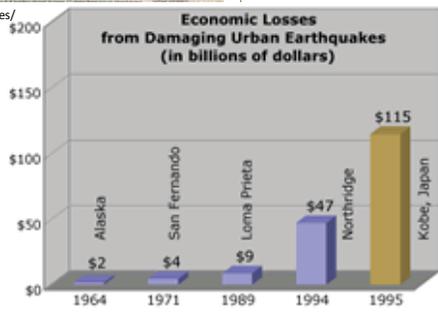
<https://www.usgs.gov/>



# Why does it matter?



<http://graphics.latimes.com/northridge-pages/>



<http://pubs.usgs.gov/fs/fs-046-03/fs-046-03.html>

# Why does it matter?

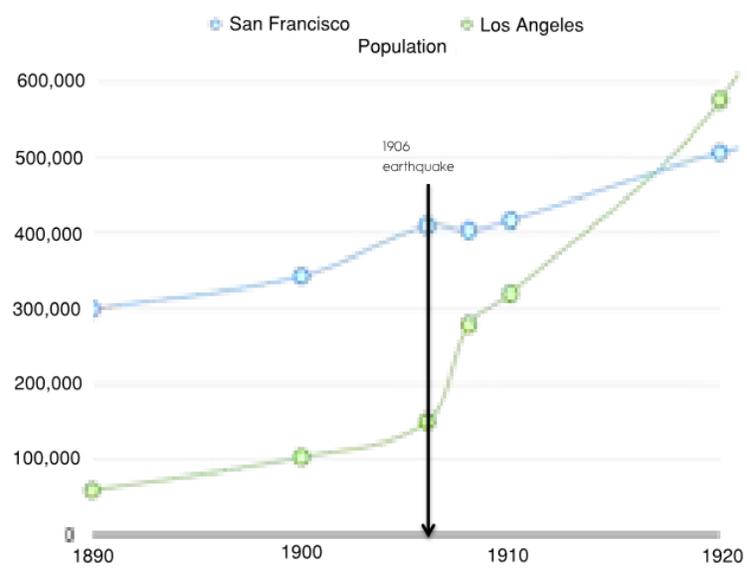


Figure 1-4. The population of the Cities of San Francisco and Los Angeles (U.S. Census Data). The population of Los Angeles grew fivefold in the decade after the 1906 earthquake struck San Francisco.

[https://d3n8a8pro7vhm.cloudfront.net/mayorofla/pages/16797/attachments/original/1420504740/Resilience\\_by\\_Design\\_Full\\_Report\\_Dec\\_11\\_FINAL.pdf?1420504740](https://d3n8a8pro7vhm.cloudfront.net/mayorofla/pages/16797/attachments/original/1420504740/Resilience_by_Design_Full_Report_Dec_11_FINAL.pdf?1420504740)

# California Code Requirements

## Additions

**3403.4 Existing structural elements carrying lateral load.** Where the addition is structurally independent of the existing structure, existing lateral load-carrying structural elements shall be permitted to remain unaltered. Where the addition is not structurally independent of the existing structure, the existing structure and its addition acting together as a single structure shall be shown to meet the requirements of Sections 1609 and 1613.

**Exception:** Any existing lateral load-carrying structural element whose demand-capacity ratio with the addition considered is no more than 10 percent greater than its demand-capacity ratio with the addition ignored shall be permitted to remain unaltered. For purposes of calculating demand-capacity ratios, the demand shall consider applicable load combinations with design lateral loads or forces in accordance with Sections 1609 and 1613. For purposes of this exception, comparisons of demand-capacity ratios and calculation of design lateral loads, forces and capacities shall account for the cumulative effects of additions and alterations since original construction.

## Alterations

**3404.4 Existing structural elements carrying lateral load.** Except as permitted by Section 3404.5, where the alteration increases design lateral loads in accordance with Section 1609 or 1613, or where the alteration results in a structural irregularity as defined in ASCE 7, or where the alteration decreases the capacity of any existing lateral load-carrying structural element, the structure of the altered building or structure shall be shown to meet the requirements of Sections 1609 and 1613.

**Exception:** Any existing lateral load carrying structural element whose demand-capacity ratio with the alteration considered is no more than 10 percent greater than its demand-capacity ratio with the alteration ignored shall be permitted to remain unaltered. For purposes of calculating demand-capacity ratios, the demand shall consider applicable load combinations with design lateral loads or forces per Sections 1609 and 1613. For purposes of this exception, comparisons of demand capacity ratios and calculation of design lateral loads, forces, and capacities shall account for the cumulative effects of additions and alterations since original construction.



**UPGRADES ARE ONLY REQUIRED WHEN SIGNIFICANT CHANGES ARE MADE TO STRUCTURE**



## Repairs

**3405.2 Substantial structural damage to vertical elements of the lateral force-resisting system.** A building that has sustained substantial structural damage to the vertical elements of its lateral force-resisting system shall be evaluated and repaired in accordance with the applicable provisions of Sections 3405.2.1 through 3405.2.3.

### Exceptions:

- Buildings assigned to Seismic Design Category A, B, or C whose substantial structural damage was not caused by earthquake need not be evaluated or rehabilitated for load combinations that include earthquake effects.
- One- and two-family dwellings need not be evaluated or rehabilitated for load combinations that include earthquake effects.

**3405.2.1 Evaluation.** The building shall be evaluated by a registered design professional, and the evaluation findings shall be submitted to the building official. The evaluation shall establish whether the damaged building, if repaired to its pre-damage state, would comply with the provisions of this code for wind and earthquake loads.

Wind loads for this evaluation shall be those prescribed in Section 1609. Earthquake loads for this evaluation, if required, shall be permitted to be 75 percent of those prescribed in Section 1613.

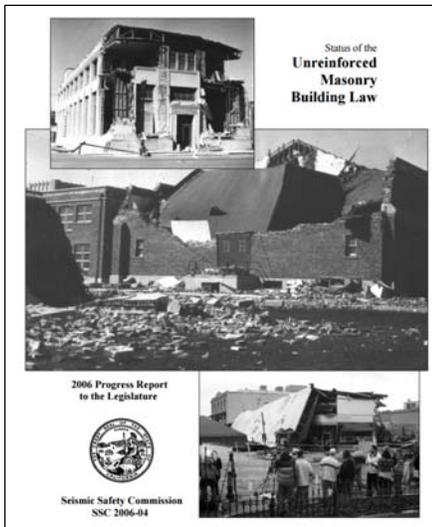
## Change in Occupancy

**3408.4 Seismic.** When a change of occupancy results in a structure being reclassified to a higher risk category, the structure shall conform to the seismic requirements for a new structure of the higher risk category.

### Exceptions:

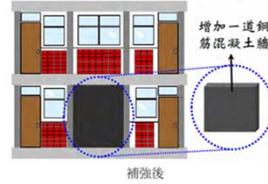
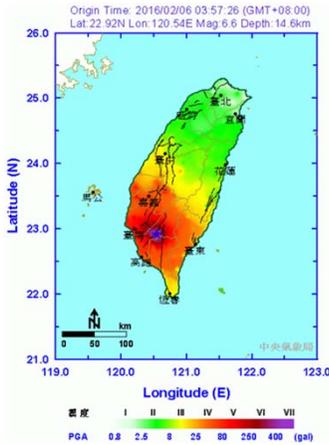
- Specific seismic detailing requirements of Section 1613 for a new structure shall not be required to be met where the seismic performance is shown to be equivalent to that of a new structure. A demonstration of equivalence shall consider the regularity, overstrength, redundancy and ductility of the structure.
- When a change of use results in a structure being reclassified from Risk Category I or II to Risk Category III and the structure is located where the seismic coefficient,  $S_{ap}$ , is less than 0.33, compliance with the seismic requirements of Section 1613 are not required.

# URM Retrofit Ordinance

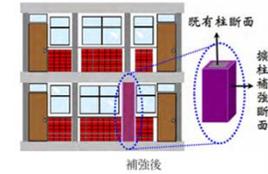
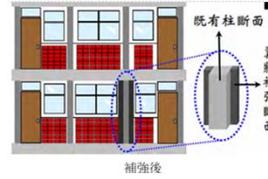


<http://www.seismic.ca.gov/pub/CSSC%202006%20URM%20Report%20Final.pdf>

# Seismic Programs Case Study



於既有框架內增設整片RC牆體，可有效提升整體結構物之強度。



## School Building Seismic Program:

- 334 "Safe" Buildings: 1 Damaged
- 75 "Unsafe" Buildings: 18 Damaged

Images provided by Justin C.H. Shih Structural Engineer & Associates 施忠賢

# Retrofit Strategies



DUCTILITY

## Retrofit Strategies



STRENGTH

## Retrofit Strategies



STRENGTH

## Retrofit Strategies



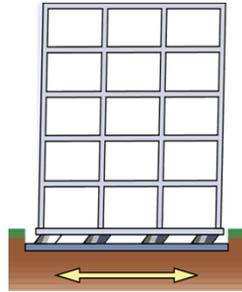
DUCTILITY

## Retrofit Strategies



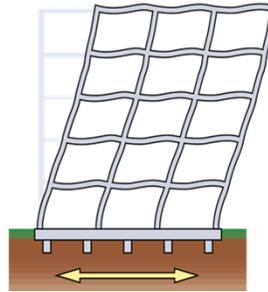
DAMPING

## Retrofit Strategies



Seismically Isolated Structure

Movement is concentrated at isolation level in seismic isolation bearings. Ideally, building above moves a rigid body with little amplification of deformations and accelerations up the height.



Conventional Structure

Buildings respond to earthquake shaking by deforming beams, columns, braces, walls. Sometimes these deformations cause damage/fracture and displacement can be permanent

### ISOLATION

## Other Considerations



### FOUNDATIONS

## Other Considerations



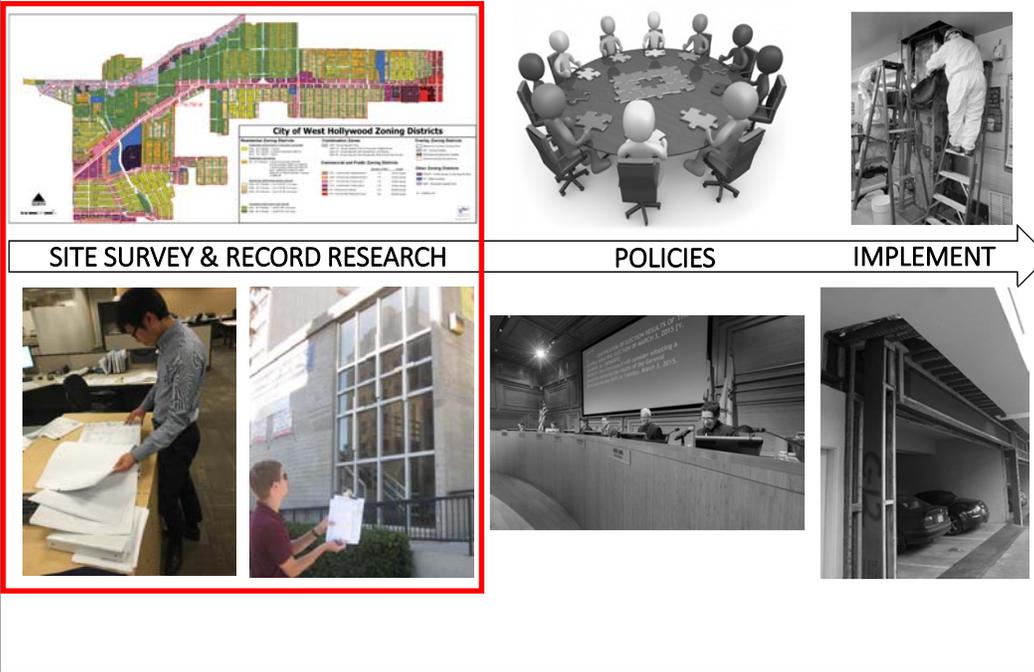
### COLLECTORS/CONNECTIONS

## Other Considerations

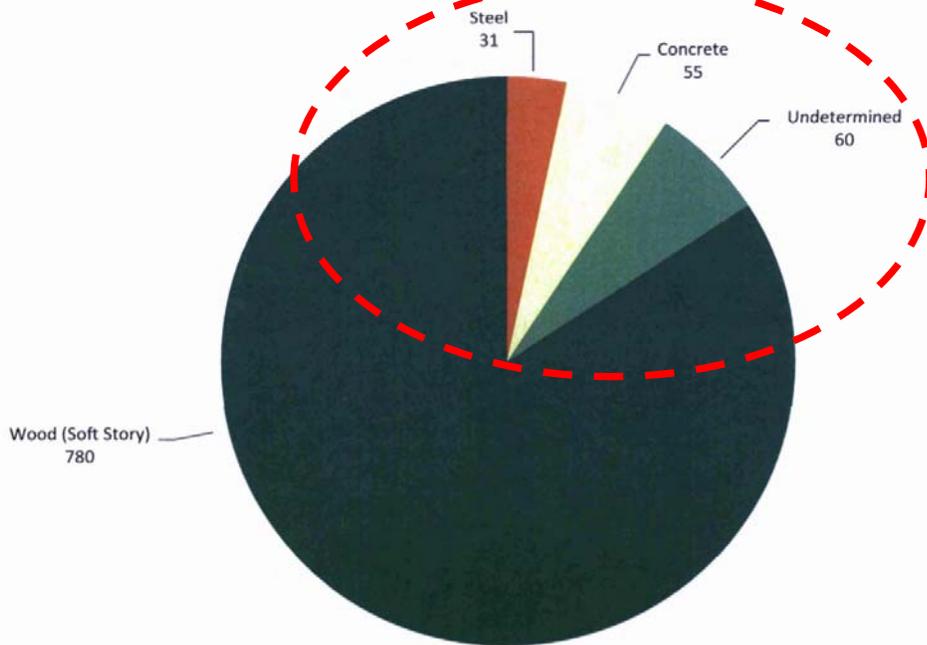


### USERS

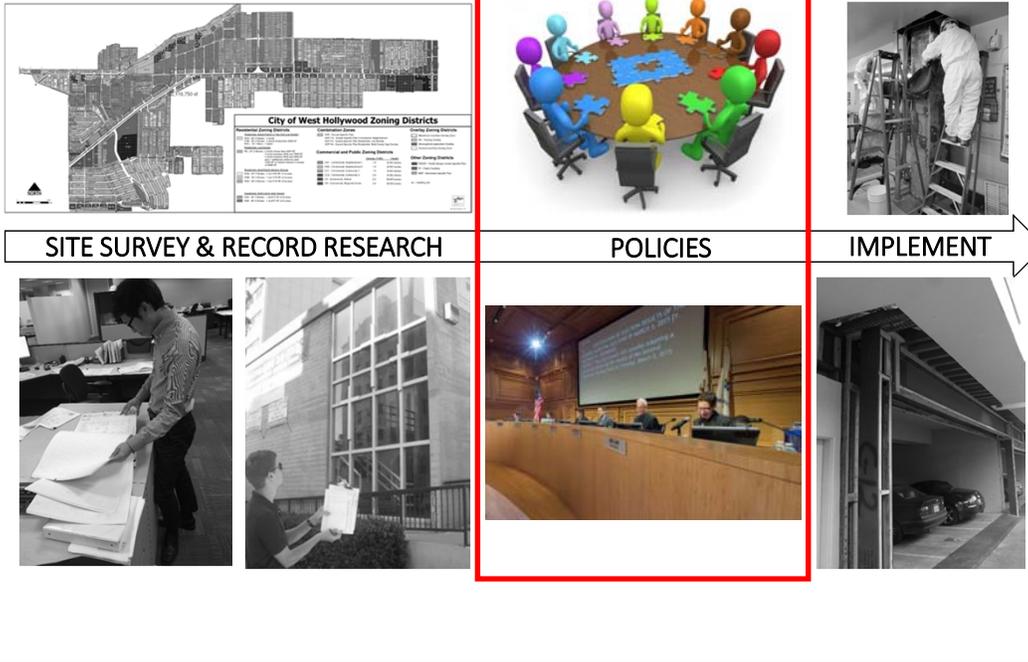
# City of West Hollywood Seismic Retrofit Program Process



## Preliminary Survey Results



# City of West Hollywood Seismic Retrofit Program Process



## Policy Considerations

FEDERAL EMERGENCY MANAGEMENT AGENCY      FEMA-107 (October 1984)  
Reprints: 500-454-8844

**Second Edition  
Typical Costs for Seismic Rehabilitation  
of Existing Buildings**  
Volume 1 - Summary

**Techniques for the  
Seismic Rehabilitation  
of Existing Buildings**  
FEMA 547/2004 Edition

**Seismic Evaluation  
and Retrofit of  
Existing Buildings**  
FEMA 446 (October 1998)  
FEMA 446 (October 1998)  
FEMA 446 (October 1998)

**ASCE**

**SEA**  
STRUCTURAL ENGINEERS ASSOCIATION  
SOUTHERN CALIFORNIA

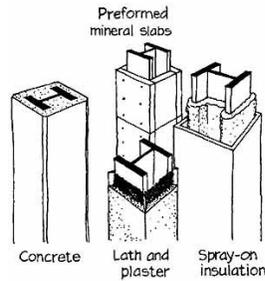
**Earthquake Safety Implementation Program**  
CAPS

# Non-Ductile Concrete Scope

**UNIFORM  
BUILDING  
CODE**



1979



13.36.020 Scope.

The provisions of this Chapter shall apply to any existing concrete building determined by the Building Official to have been built under Building Code standards enacted before the 1979 Uniform Building Code with local amendments.

Exceptions: This Chapter shall not apply to the following structure types:

1. Concrete structures with flexible diaphragms.
2. Single Story structures, unless the lateral system contains concrete moment frame elements.
3. Wood structures over concrete podium unless the podium contains a Major Deficiency as specified in section 13.36.050.a.
4. Buildings with a steel lateral resisting system encased in concrete.



# Pre-Northridge Steel MF Scope

13.40.020 Scope.

The provisions of this Chapter shall apply to any building utilizing a Steel Moment Frames that are determined by the Building Official to have been built under building code standards enacted before December 1995.

This Chapter shall not apply to the following structure types:

1. Unreinforced Masonry Buildings previously strengthened with Steel Moment Frames
2. Residential Wood-Framed Buildings utilizing Steel Moment Frames.

Notwithstanding any provision of the Building Code, compliance with this Chapter shall not require existing electrical, plumbing, mechanical or fire-safety systems to be altered to comply with the current Building Code unless they constitute a hazard to life or property as determined by the Building Official.



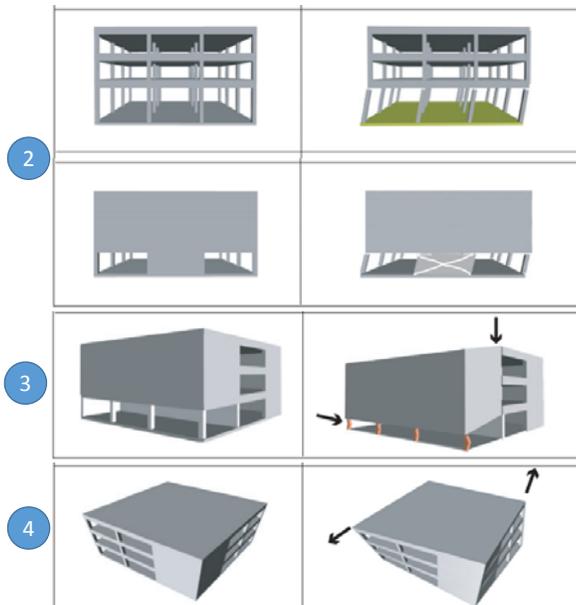
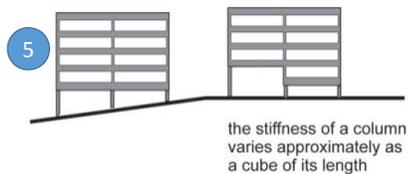
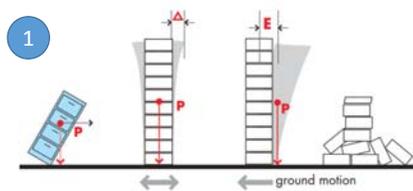
# Proposed Policy

Policy Items	Los Angeles	West Hollywood
Voluntary or Mandatory Retrofit	Mandatory	Mandatory
Timelines	25 Years for Full Retrofit of 1,500 Bldgs	10 Years for Major Deficiency Retrofit and 10 Additional Years for Full Retrofit of ~146 Bldgs.
Priority Tiers	3 Tiers	3 Tiers
Incentives and Facilitation Programs	Financial programs are being explored	Financial programs are being explored
Architectural Improvements	Waived with exception of ADA	Waived with exception of ADA
MEP Improvements	Waived	Waived

# Major Deficiencies

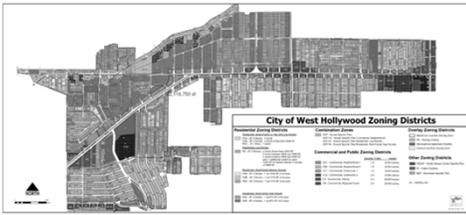
**Major Deficiencies:**

1. Load Path
2. Weak or Soft Story
3. Vertical Irregularity
4. Torsion
5. Captive Column



[https://www.fema.gov/media-library-data/20130726-1556-20490-5679/fema454\\_complete.pdf](https://www.fema.gov/media-library-data/20130726-1556-20490-5679/fema454_complete.pdf)

# City of West Hollywood Seismic Retrofit Program



SITE SURVEY & RECORD RESEARCH

POLICIES

IMPLEMENT



## Implementation



# Summary

TABLE A

TIME PERIOD FOR COMPLIANCE

Phase	Phase 1: Engineering Report & Major Deficiency Mitigation <sup>a, b</sup>				Phase 2: Complete Retrofit <sup>d</sup>		
	Submit Engineering Report & Determine All Structural Deficiencies	Submit Retrofit Plans for Major Deficiency Mitigation	Obtain Building Permit & Commence Construction	Complete Major Deficiency Mitigation Construction <sup>c</sup>	Submit Retrofit Plans	Obtain Building Permit & Commence Construction	Complete Construction
Milestone	3 Years from notice to the Owner	5 Years from notice to the Owner	7 Years from notice to the Owner	10 Years from notice to the Owner	13 Years from notice to the Owner	15 Years from notice to the Owner	20 Years from notice to the Owner

a. All buildings within the scope of this Chapter are required to submit an engineering report & determine all structural deficiencies. Buildings that do not contain any of the Major Deficiencies as defined in this Chapter are not required to submit Retrofit plans for Major Deficiency mitigation, commence construction, and complete construction in Phase 1, but shall provide Retrofit plans and complete construction within the time limits provided in Phase 2.

b. Phase 1 Retrofit plans must indicate preliminary Phase 2 Retrofit extents. Minimum Phase 2 scoping requirements shall be as specified by the Building Official.

c. Completion of Phase 1 may be extended by 3 years if Retrofit plans in accordance with the scope of Phase 2 are designed, approved, permitted and constructed within Phase 1.

d. The Building Code version governing Phase 1 shall be permitted to be utilized in Phase 2.

TABLE B  
PRIORITY DESIGNATION

Priority	Description
Priority I.	Buildings with 8 or more stories
Priority II.	Buildings with 3 to 7 stories
Priority III.	Buildings with 2 or less Stories

Let's **Talk**  
about it



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